## An Investigation of Alternative Lighting and Electrical Systems With Additional Mechanical and Acoustical Studies



Villanova University: School of Law
Villanova, PA

Jason Greer
Lighting/Electrical Option
Lighting Consultant: Dr. Kevin Houser
Electrical Consultant: Professor Ted Dannerth

April 09, 2008

## the people

owner: villanova university general contractor: gilbane cm: smithgroup architect: smithgroup mep: smithgroup landscape architect: ml baird \& co civil engineer: yerkes associates inc structural engineer: o' donnell \& naccarato inc

## the statistics

size: 170,000 sf
levels: 3 above grade/ 1.5 below grade construction begins: November 2, 2007 owner occupancy: August 20, 2009
project delivery method: GMP
cost: $\$ 56.5 \mathrm{M}$ estimated total construction cost


## mechanical

- 1 300-ton water-cooled, centrifugal chiller and 1300 -ton two-stage direct fired twostage absorption chiller located in lower level main mechanical room system with a 15 kV primary loop switch
- 1 primary, constant volume, endsuction chilled water pump for each chiller
- 2 secondary chilled water pumps will distribute water at 42 deg $F$ to cooling coils throughout building
- heat will be provided using campus central steam plant


## structural

foundations: columns will bear on spread footings columns: wide flange w/ a typical size of W12×72 ground floor: the ground floor will be SOG floor framing: composite structural steel wide flange beams and girders supporting light weight concrete on metal deck
floor framing: w-beams and girders supporting wide rib metal deck

## Table of Contents

Executive Summary ..... 3
Introduction, Background \& Building Overview ..... 4
Lighting Depth ..... 8
Courtyard ..... 10
Atrium ..... 20
Atrium Daylighting ..... 32
135-Seat Classroom ..... 42
Moot Court ..... 56
Electrical Depth ..... 70
Electrical Coordination of Lighting Design ..... 71
Distribution System Redesign ..... 111
Atrium HVAC Equipment Redesign ..... 159
Energy Efficient Transformer Study ..... 165
Protective Device Coordination ..... 169
Mechanical Breadth ..... 172
Acoustical Breadth ..... 177
Summary \& Conclusions ..... 182
References ..... 184
Acknowledgements ..... 185
AppendicesAppendix A
Appendix B
Appendix C
Appendix D
Appendix E

## Executive Summary

The Villanova University School of Law thesis project looked at a number of different system redesign and how each would affect the existing systems in the building, the energy properties, the initial and long term cost as well as other construction issues.

The lighting depth focused on the redesign of four spaces in the law school. The four spaces that were redesigned were the courtyard, the atrium, the 135 -seat classroom and the moot courtroom. Each design was created in accordance with the criteria set fourth by the IESNA Lighting Handbook and ASHRAE 90.1. The lighting designs for the interior of the building were designed to be flexible, functional educational spaces with an emphasis on some of the key architectural elements. The more exterior spaces were designed to shine like a beacon at night for the rest of the campus to see. As a part of the lighting depth, a daylight study was done for the atrium to determine the benefits of specifying a new glazing system.

The electrical depth focused on the coordination between the new lighting systems and the existing electrical system. This was done through panelboard, feeder, and over-protection sizing. Another area of focus in the electrical depth was the redesign of the distribution system. A more centralized system was explored which implements distribution panels to feed panels rather than lighting and receptacle panels feeding other lighting and receptacle panels. This resulted in a reduction of the number of transformers. A cost analysis was done comparing the new and old systems to determine the best option for the law school. The other areas the electrical depth focuses on are a redesign of the power supply to a rooftop air handling unit that was resized per the mechanical breadth, a payback study to determine the feasibility of implementing energy efficient transformers over standard K-rated transformers and lastly an over-current device coordination study was done on one path through the building.

A mechanical analysis was studied as a breadth topic. The focus of this was determining the mechanical load reduction that resulted from specifying new glass in the atrium. A cost analysis was done to determine how much the new system would cost initially and what kind of energy saving would result.

The final study in this report is an acoustical study that focuses on the 135-seat classroom and the moot courtroom. Initial reverberation time was calculated and materials were modified as a result in an effort to get the reverberation time within the recommended range. Finally, a cost analysis was performed to determine the cost of getting these spaces to fall within the recommended reverberation time range.

## Introduction \& Background

The Villanova University School of Law is a 170,000 square foot facility that integrates classrooms, student services, a law library, faculty offices, administrative offices, dining facilities and a legal clinic into a single state of the art facility. Construction was set to begin in November of 2007 with owner occupancy being set for August of 2009. Upon completion, the building will provide a centralized space for law students and faculty to complete their work.

## Building Overview

Building Name: Villanova University: School of Law
Location and Site: Villanova University campus, Villanova, PA.
Building Occupant: Villanova University: School of Law
Occupancy \& Function:
Library, classrooms, student services, faculty and administrative offices, chapel, dining facilities and legal clinic.

Size: 170,000 SF

## Number of Stories:

Three stories above grade. Two stories below grade (basement, sub-basement).
Primary Project Team:
Owner: Villanova University
General Contractor: Gilbane
CM: SmithGroup
Architect: SmithGroup
MEP: SmithGroup
Landscape Architect: ML Baird \& CO Landscape Architects
Civil Engineer: Yerkes Associates, Inc.
Structural Engineer: O'Donnell \& Naccarato, Inc.
Construction Dates: November, 2007 through August, 2009.

## Cost Information:

Estimated total construction cost including accepted value engineering: $\$ 56.57 \mathrm{M}$
Project Delivery Method: Guaranteed Maximum Price (GMP)

## Architecture:

The building is organized in two " $L$ " shaped plans which create a three sided courtyard that faces west. One wing or "L" is occupied entirely by the law library, faculty offices, and the chapel. The other wing houses the classrooms, the atrium, the dining facility and other student activity areas. The floor to floor height for the law library and offices is a typical 14' while the classrooms on the first, second and third floors have a floor to floor height of 17 ' which allows for the tiered classrooms.

## Major National Codes: IBC 2003

## Building Envelope:

Punched windows will be constructed of 5" deep extruded aluminum frames with 1 " insulated low-e glazing.

The window-wall system will be constructed of 7.5 " aluminum mullions with 1" low-e glazing units and opaque spandrel glass units. Portions of the glazing on the atrium will be fitted with a ceramic frit screen pattern.

The roof will be constructed of a modified bitumen system over corrugated structural roof deck. The steel structure will be sloped to roof drains located along the center bay of each wing. There will be tapered insulation crickets to direct rain water toward drains between collection areas.

The roof assembly will consist of the following:

- $\quad$ Structural steel deck
- 4" rigid insulation pinned to deck
- 1 " recover board adhered to insulation
- Modified base sheet adhered to recover board
- Modified roof membrane and cap sheet adhered to base sheet


## Structural System:

The structural system consists of spread footings that will bear the columns. The columns are 12 " deep wide flange with a typical size of $\mathrm{W} 12 \times 72$. The ground floor is SOG while the other floors are typical elevated floor framing and is constructed of composite structural steel wide flange beams and girders supporting 3-1/4" light weight concrete. The concrete is placed on top of composite metal deck with a span width of $8^{\prime}$. The roof framing consists of wide flange structural beams and girders supporting galvanized wide rib metal deck. The steel beams are spaced 6' o.c.

## Electrical:

The power distribution system for the Villanova University School of Law is a simple radial system. The electric service is connected to the university's 13.2 Kv underground primary distribution system with a 15 Kv primary loop switch. The service is provided by a $2000 \mathrm{Kva}, 13.2 \mathrm{Kv}$ primary voltage to $480 \mathrm{Y} / 277 \mathrm{~V}$ secondary voltage, 3 phase, 4 wire transformer located outside the building. A 3000A, $480 \mathrm{Y} / 277 \mathrm{~V}, 3$ phase, 4 wire switchboard is located in the sub-basement and will distribute power to
the building. The switchboard provides power to elevators, the chiller plant, AHUs, and the lighting and receptacle panels. The receptacle panels are supplied through 480 V to 208 V transformers.

## Lighting:

In an ongoing effort to lessen the impact construction has on the environment, the law school utilizes mostly fluorescent lighting. In the larger spaces (i.e. classrooms, lecture spaces, courtrooms and the stacks in the library) fluorescent pendant lighting is used to provide the ambient lighting. In smaller spaces such as faculty offices and egress corridors, recessed compact fluorescent luminaires are used. In areas of interest throughout the building, some incandescent lighting is used. In the hallways, there are coves above each door which are illuminated with tubular fluorescent luminaires that draw your eye to the entrance of the space.

Occupancy sensors are used as a way to ensure that energy is not used during unnecessary times. Some spaces have time switches at the entrance that serve the same purpose. These spaces are mostly spaces that are not used for extended periods of times. Photocells have been utilized in areas with a large amount of glazing. This is yet another way to ensure that all possible energy savings are taken advantage of.

In addition to these localized controls, the building has three lighting control panels that control the times of operation of the lighting throughout the building. Spaces such as offices are turned on at 8 am and shut off at 6 pm , unless of course the occupancy sensor prevents it. The areas that will be used by students for longer periods of time will be switched on at 7 am and shut off at 10 pm . Again this will not affect a space if it is being used because the occupancy sensors will relay that information back to the LCP.

## Mechanical Cooling:

The Villanova University School of Law utilizes one 300-ton water-cooled, centrifugal chiller and one 300-ton two-stage direct fired absorption chiller which are located in the lower level main mechanical room. The chilled water system is a primary-secondary system. One primary constant volume, base-mounted, end suction chilled water pump is provided for each chiller. Two secondary, variable volume, base-mounted, end-suction chilled water pumps are provided and each is sized for $100 \%$ flow.

Two induced-draft, cross flow, single-cell cooling towers are located on the roof. Each tower serves an individual chiller. One serves the absorption chiller and is sized at $4.0 \mathrm{gpm} / \mathrm{ton}$. The other tower serves the centrifugal chiller and is sized at $2.5 \mathrm{gpm} / \mathrm{ton}$.

## Mechanical Heating:

Heat is provided using Villanova University's central steam plant. Steam is provided year round to the facility. A 4-inch, 125 psig steam line enters the main mechanical room on the lower level. The steam line is sized to provide approximately $10,350 \mathrm{MBH}$ or $8,990 \mathrm{lb} / \mathrm{hr}$.

## Fire Protection:

The fire alarm system is a solid state, multiplex, addressable fire alarm system that consists of graphic annunciation panels at the entrance lobby. Manual pull stations, audio/visual devices, flow switches, tamper switches and smoke and heat detectors are located throughout the building.

The fire alarm system is connected between the building security system and the campus central security console. The fire alarm system can be monitored through any computer and a printer can output all fire alarm activity. The smoke and heat detectors for the elevator system are interfaced with the elevator controllers for elevator recall and shut down requirements.

## Telecommunications:

A duct bank for telecommunication service to the law school is provided from Villanova University's campus telecommunication network. A main telecom demarcation room is located in the basement. Two telecom rooms are located on each additional floor. A complete telecom raceway system consisting of back boxes, conduits, and ladder trays are run throughout the building on each floor.

All voice and data cables are provided by others as part of a separate contract. Card access system equipment is also provided as part of a separate contract.

Finally, a complete security raceway system is provided throughout the building where needed.

## Transportation:

The main stair case is located at the meeting point of the two wings of the law school. Located beside this main stair case are the three main elevators that serve all levels. At each end of the two wings there is a small stair case that serves each floor as well. There are no elevators in these areas however.

## Lighting Depth

## Introduction

The Villanova University School of Law has been designed to be a hub for legal studies. Students and faculty alike will have the privilege to access the brand new law library, moot courtroom, classrooms and computer labs. Aside from learning, there are many student service spaces to be taken advantage of. Because of these excellent features, the law school should be a building that makes a statement both inside and out. Ideally, students and faculty will be welcomed upon arriving at the building through the architecture and lighting, and be in no hurry to leave once inside.

The lighting depth focuses on the creation and analysis of lighting designs for the following spaces:

1. Courtyard
2. Atrium adjacent to the courtyard
3. 135-Seat Classroom
4. Moot Courtroom

The lighting analysis for each space discusses goals, design criteria, controls, performance and power density. Each space that was redesign was done so in accordance with the ASHRAE 90.1 space by space method for calculating power densities.

In addition to the analysis for each lighting design, a daylight study is done for the atrium. This space has a significant amount of glazing and as part of the mechanical breadth, that glazing was replaced in hopes of achieving better mechanical performance. The two types of glazing are studied from a daylight standpoint in the lighting section of this report.

## COURTYARD

## Introduction

Upon arriving at the Villanova University School of Law, the first space one will encounter is the courtyard. The main function of the courtyard is a circulation space. People will mostly walk from their car into the law school through the courtyard. Aside from the circulation of pedestrians, this space has the opportunity to offer a greeting to all guests. The atrium just beyond makes the space quite interesting and inviting. Because of this, the lighting in the courtyard will be subtle, with just enough light to provide adequate security for persons walking through. This will allow the atrium to make its statement.

## Space Layout

The following figure illustrates the layout of the courtyard. The bottom of Figure 1.1 would be the parking lot, and one would progress to the building from there.


Figure 1.1.1 - School of Law Courtyard

## Architectural Finishes

Walkways


Unfinished Concrete
Gray
Reflectance: 35\%


Unfinished Limestone
Tan
Reflectance: 35\%

## Building Façade



Mullions
Dark Gray
Reflectance: 10\%


Brick
Beige
Reflectance: 39\%


Brick
Red
Reflectance: 24\%


Unfinished Limestone
Tan
Reflectance: 35\%


Fieldstone
Gray
Reflectance: 29\%

## Target Illuminance Values

Entrance - 5 fc horizontal
Walkways - 1-5fc

## Design Criteria

- Appearance of Space and Luminaires (Important)

This space needs to portray the same excellence that the spaces do inside. The luminaires need to be high quality and architecturally attractive. While the space as a whole must be attractive, the space must not take away from the atrium, which is the true focal point.

- Color Appearance (Important)

Color rendering is important in terms of façade lighting and landscape lighting. The space will be relatively dark, but the accents need to bring out the colors of the materials being accented.

- Daylighting Integration and Control (Somewhat Important)

The lighting should only be on when it is needed.

- Direct Glare (Important)

This will most likely not be an issue because of the luminaires selected. The low height bollards and the high mounted accent lights will not have a glaring effect.

- Light Distribution on Surfaces (Important)

There is a fair amount of glazing so façade lighting will be limited. However, where there is façade lighting, it is important that it gives the intended effect.

- Uniform Light Distribution on Task Plane (Not Important)

The main goal of this space is to provide a safe environment to walk from the parking lot to the building or vice versa. Uniform lighting over the whole space is not necessary.

- Modeling of Faces (Not Important)

This space will rarely be used at night other than for walking purposes. Rarely will a person be in the space for an extended period of time during the evening. The one space people could be for a longer time is near the entrance. In that area, a fair amount of light will be leaking from the atrium which will help with facial rendering.

- Points of Interest (Not Important)

The biggest point of interest in the courtyard will be the glass atrium. This will be illuminated from the inside so there is no need to try to put focus on something else in the space.

- System Control and Flexibility (Important)

It is important that the luminaires in the courtyard are burning only when it is dark out. This is accomplished using a time clock system.

The overall design goal of this space is to provide a space with adequate security lighting and still allow the atrium to dominate. The focus upon arriving at the school of law should be the atrium which lies directly beyond the courtyard.

## Luminaire Schedule

| Image | Tag | Description | Volt | Manuf. | Cat. No. | Lamp |  | Mounting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | No. | Type |  |
| $\square$ | F2a | Recessed Downlight (Wet) | 277 | Zumtobel | S5D7704-U-7703L-C | 2 | $\begin{aligned} & \hline 26 \mathrm{~W} \\ & \mathrm{CFL} \end{aligned}$ | Recessed |
|  | H1 | 32" Full Cutoff Bollard | 277 | Erco | 33353.023 | 1 | $\begin{aligned} & \text { 70W } \\ & \text { MH } \end{aligned}$ | Surface |
|  | H3 | $11 "$ <br> Cylinder <br> Downlight | 277 | Gotham | CW11100MCAR277 | 1 | $\begin{aligned} & \text { 100W } \\ & \text { MH } \end{aligned}$ | Wall |
|  | H4 | Landscape Flood | 277 | Allscape | $\begin{aligned} & \text { Sl-51-20MH-PAR20-277- } \\ & \text { FLD-BK } \end{aligned}$ | 1 | $\begin{aligned} & \text { 20W } \\ & \text { MH } \end{aligned}$ | Tree |
|  | H6 | Surface <br> Mount <br> Projector | 277 | Lumiere | 710MH39PAR20277WRBK | 1 | $\begin{aligned} & \text { 20W } \\ & \text { MH } \end{aligned}$ | Surface |

Table 1.1.1 - Courtyard Luminaire Schedule
*See Appendix A for all ballast, and luminaire cut sheets.

## Lighting Layout



Figure 1.1.2 - Courtyard Lighting Plan
Full-size plan located in Appendix B

## Controls

The controls for the courtyard are 100 percent time based. As an effort to save energy and reduce electricity costs, all luminaires will be controlled using a time clock. Each day all luminaires will switch on at sunset and switched off at sunrise the next morning. The law school was originally designed with a control panel designated to do the same thing with the exterior lighting and this system will simply be circuited to the existing control system. Please refer to electrical depth page 73 for control details.

## Light Loss Factors

| Tag | Descr. | Dirt | Exposure | LDD | LLD | BF | LLF |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Recessed <br> Downlight <br> (wet) | Dirty | 1 Year | 0.80 | 0.88 | 0.95 | $\mathbf{0 . 6 7}$ |
| H1 | Bollard | Dirty | 3 Years | 0.77 | 0.81 | 1.00 | $\mathbf{0 . 6 2}$ |
| H3 | 11" Cylinder <br> Downlight | Dirty | 3 Years | 0.77 | 0.67 | 1.00 | $\mathbf{0 . 5 1}$ |
| H4 | Landscape <br> Flood | Dirty | 3 Years | 0.77 | 0.71 | 1.00 | $\mathbf{0 . 5 5}$ |
|  | Surface <br> H6 <br> Landscape <br> Projector | Dirty | 3 Years | 0.77 | 0.71 | 1.00 | $\mathbf{0 . 5 5}$ |

Table 1.1.2 - Courtyard Light Loss Factors

## Power Density

| Room: | Courtyard | Desired WP FC: | 1-5fc |  |
| :---: | :---: | :---: | :---: | :---: |
| Square Footage: | 24014 | Ashrae Allow: | 0.2 |  |
| Total Watts Allowed: | 4802.8 |  |  |  |
| TAG | DESCRIPTION | WATTS | NO. USED | TOTAL WATTS |
| F2a | Recessed Downlight (Outdoor) | 34 | 11 | 374 |
| H1 | Bollard | 94 | 19 | 1786 |
| H3 | 11" Cylinder Downlight | 129 | 13 | 1677 |
| H4 | Landscape Flood | 26 | 7 | 182 |
| H6 | Exterior Surface Mount Projector | 53 | 4 | 212 |
| TOTAL ROOM WATTS: ROOM WATTS REMAINING: | $\begin{aligned} & 3857 \\ & 945.8 \end{aligned}$ | Power Density: Actual to Allowed: | $\begin{array}{r} \mathbf{0 . 1 6} \\ 80.31 \% \\ \hline \end{array}$ |  |

## Table 1.1.3 - Courtyard Power Density

The courtyard uses roughly 80 percent of the energy allowed by ASHRAE 90.1. Therefore, this design is acceptable and if there were spaces elsewhere in the building that do not meet their specific power density requirements, the leftover watts from this space would be helpful.

## Design Performance

While the safety of pedestrians at night is the number one priority in this space, that can be accomplished with fairly low light levels. The IES recommendation for illuminance levels for a walkway is between one and five foot-candles.

The lighting design for this space was fairly simple. Bollards are used to light the walkway that winds around the grassy area of the courtyard. Façade lighting, and light from inside light the patio. There is a single landscape luminaire mounted in each of the seven trees to provide some accent and more interest to the center of the courtyard.

| Courtyard Illuminance Data (fc) |  |  |  |
| :--- | ---: | :--- | ---: |
| Patio |  |  |  |
| Average | 6.01 | Average | 3.07 |
| Max | 19.4 | Max | 6.7 |
| Min | 0.9 | Min | 0.5 |
| Avg/Min | 6.68 | Avg/Min | 6.14 |
| Max/Min | 21.56 | Max/Min | 13.4 |

Table 1.1.4 - Courtyard Illuminance Data
The farther walkways were not reported in numerical form due to the difficulty of placing a calculation plane on a sloped surface. The illuminance values will be similar to what was reported above based on similar spacing. The next image shows a pseudo color renderings which illustrates all walkways illuminance levels.

## Renderings



Image 1.1.1 - Courtyard Plan View Pseudo Color Rendering
Image 1.1.1 shows that the walkways are between 1 fc and 5 fc in most locations.


Image 1.1.2 - View from parking lot


Image 1.1.3 - View from center of courtyard


Figure 1.1.4 - View of entrance


Image 1.1.5 - Raytraced image from center of courtyard

## Conclusion

The courtyard successfully provides a safe passage way from the parking lot to the entrance of the law school. The lighting design is subtle enough as to not take away from the glowing atrium just beyond it. The accented trees provide some excitement in the center of the courtyard just before you reach the atrium. This is an exterior that provides the necessary safety lighting while drawing one toward the corner stone of the law school's lighting design.

## ATRIUM

## Introduction

The atrium is the predominant feature that will be seen when arriving at the law school. In the evening hours, the atrium will glow from within. The atrium will draw attention to the building's entrance and leave no question of where to enter. This space will be used mainly as a transition space as it connects the two wings of the law school. There is some seating in the atrium but the majority of users will simply pass through the space.

## Space Layout



Figure 1.2.1 - Atrium Floor Plan (original floor design)


Figure 1.2.2 - Atrium Floor Plan


Figure 1.2.3 - Atrium North-West Elevation


Figure 1.2.4 - Atrium South-East Elevation

## Architectural Finishes

Floor


Carpet
Beige/Gray
Reflectance: 37\%

Walls


Painted Gyp Board
White
Finish: Matte
Reflectance: 95\%

Painted Gyp Board
White
Finish: Matte
Reflectance: 82\%


Wood Paneling
Light Stain
Reflectance: 42\%

## Ceiling

Painted Gyp Board<br>Heron White<br>Finish: Matte<br>Reflectance: 92\%

## Design Goals

The main goal in the atrium is to provide a space that attracts the attention of passersby in the evening hours. The atrium will glow and serve as a beacon of the new campus skyline. The wood panels in the atrium are the predominant feature of the space and will be accented. This space will guide people, both from outside to in, and from wing to wing. Photo sensors will be used to control the lighting when there is ample daylight entering the space.

## Target Illuminance Values

Floor - 10 fc (horizontal)

## Design Criteria

- Appearance of Space and Luminaires (Important)

This space will be the focal point of the law school. The appearance of the space and luminaires is important. The atrium is going to make the first impression to all who enter the law school and all aspects should be attractive.

- Color Appearance (Important)

The color appearance of the space and luminaires is important. There are very prominent wood panels in the space. The luminaires being used have good color rendering characteristics which will allow the wood to be accented properly.

- Daylighting Integration and Control (Important)

This is the space in the building that has the most daylight entering and therefore requires the most control. The daylight entering the space gives the opportunity to shed some lighting load during sunny days but it also provides a problem in terms of lighting lexibility. Shutting off certain lights to allow the natural light to illuminate the space is a must in today's construction world.

- Direct Glare (Somewhat Important)

In a space like this, direct glare is usually not an issue because of the mounting height. In a double high space, it will be hard to have direct glare because of the distance away from the people in the space as they will not likely be looking straight up very often. However, it has to be addressed that the people overlooking the space may have a more direct line of sight to the light sources. In that case, direct glare must be considered more closely.

- Light Distribution on Surfaces (Very Important)

The surfaces in this space need to be illuminated correctly to avoid undesired results. The wood on the walls needs to be illuminated well in order to allow the wood to stand out and compliment the rest of the room in the desired way. Lighting the surfaces is also what is going to allow the atrium to glow at night and be seen from the outside.

The glass façade is a surface that should also be addressed. It is important that the light that is intended to bring out the architecture does not produce strong reflections and glaring situations. Strong glare and reflections can ruin the comfort of any space.

- Uniform Light Distribution on Task Plane (Somewhat Important)

The task plane in this space is going to be the floor. The floor obviously needs enough light to for people walk through the space comfortably and most importantly safely. Because people will either be walking through or reading leisurely, the ambient light level can be lower than it would be for typical reading tasks (approximately 10 fc ) and does not need to be totally uniform.

Secondly, this is a space that will serve as a relaxing space in the evenings and uniform light levels will not provide such a space. Non-uniform lighting along the periphery will provide the greatest degree of relaxation.

- Points of Interest (Important)

The points of interest in the atrium are the wood panels that will be accented. From the outside, the atrium as a whole will be serving as the point of interest.

- Surface Characteristics (Important)

The amount of wood in this space requires attention. Illuminating the wood will be attractive to those in the space, but more importantly allow the space to glow from the outside and draw the attention of those passing by.

- System Control (Important)

It is important that this space be controlled when it comes to daylight. With the large amount of glazing, many times throughout the year, the lights in this space will not need to be switched on. Automatic switching will be done using photo sensors.

## Luminaire Schedule

| Image | Tag | Description | Volt | Manuf. | Cat. No. | Lamp |  | Mounting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | No. | Type |  |
|  | F2 | Recessed Downlight | 277 | Zumtobel | S5D-U-6308R-C | 1 | $\begin{aligned} & \hline 32 \mathrm{~W} \\ & \mathrm{CFL} \end{aligned}$ | Recessed |
|  | F5 | Cove Light | 277 | Lightolier | CL-1-4-T5-2 | 1 | $\begin{aligned} & 28 \mathrm{~W} \\ & \text { T5 } \end{aligned}$ | Surface |
|  | F8 | Recessed <br> Linear <br> Fluorescent WW | 277 | Focal Point | $\begin{aligned} & \text { FAVA-NS-1T5-1C- } \\ & \text { 277-S-F } \end{aligned}$ | 1 | $\begin{aligned} & 28 \mathrm{~W} \\ & \text { T5 } \end{aligned}$ | Recessed |
|  | H2 | 11" Cylinder Downlight | 277 | Gotham | CW11100MCAR277 | 1 | $\begin{aligned} & \text { 100W } \\ & \text { MH } \end{aligned}$ | Pendant |
|  | H5 | Surface <br> Mount <br> Projector | 277 | Se'lux | $\begin{aligned} & \text { PRO20-SM- } \\ & \text { HO70T6-830-BK- } \\ & 277-\text { FG } \end{aligned}$ | 1 | $\begin{aligned} & \hline 70 \mathrm{~W} \\ & \text { CMH } \end{aligned}$ | Surface |

Table 1.2.1 - Atrium Luminaire Schedule

Lighting Layout


Figure 1.2.5 - Atrium Lighting Layout

## Controls

The atrium is controlled using a dimming controller with a photo sensor such as the WattStopper LightSaver LCD-203 Dimming Controller. This dimmer can control three zones each of which can be dimmed or switched. The pendant HID fixtures will be simply switched on or off depending on the amount of daylight in the space. The fluorescent lighting will dimmed based on the daylight. Please refer to electrical depth page 85 for control details.

## Light Loss Factors

| Tag | Descr. | Cat. | Class | Dirt | Cleaning | LDD | RSDD | LLD | BF | LLF |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F2 | Recessed Downlight | VI | Direct | Clean | 12 mos . | 0.88 | 0.98 | 0.84 | 0.95 | 0.69 |
| F5 | Cove Light | V | Indirect | Clean | 12 mos . | 0.88 | 0.92 | 0.92 | 1.00 | 0.74 |
| F8 | Recessed Linear <br> Fluorescent WW | V | Direct | Clean | 12 mos . | 0.88 | 0.97 | 0.92 | 1.00 | 0.79 |
| H2 | 11" Cylinder Downlight | IV | Direct | Clean | 12 mos . | 0.88 | 0.97 | 0.72 | 1.00 | 0.62 |
| H5 | Surface <br> Mount <br> Projector | V | Direct | Clean | 12 mos . | 0.88 | 0.97 | 0.71 | 1.00 | 0.61 |

Table 1.2.2 - Atrium Light Loss Factors

## Power Density

| Room: | Atrium | Desired WP FC: | 10 |  |
| :---: | :---: | :---: | :---: | :---: |
| Square Footage: | 3274 | Ashrae Allow: | 1.2 |  |
| Total Watts Allowed: | 3928.8 |  |  |  |
| TAG | DESCRIPTION | WATTS | NO. USED | TOTAL WATTS |
| F2 | Recessed Downlight | 36 | 12 | 432 |
| F5 | Cove Light | 34 | 12 | 408 |
| F8 | Recessed Linear Fluor. Wall Wash | 37 | 6 | 222 |
| H2 | 11" Cylinder Downlight | 129 | 7 | 903 |
| H5 | Surface Mount Projector | 94 | 6 | 564 |
| TOTAL ROOM WATTS: | 2529 | Power Density: Actual to Allowed: | 0.77 |  |
| ROOM WATTS REMAINING: | 1399.8 |  | 64.37\% |  |

Table 1.2.3 - Atrium Power Density
The atrium uses roughly 65 percent of its allowed 3929 watts. By hitting the target illuminance levels and obtaining the intended design while staying under the required power density the law school can either use those watts in another space that needs them, or it can simply use the unused watts to lessen its environmental impact.

## Design Performance

The target illuminance level for the atrium was 10 fc . Since the space is used primarily as a transition space, a low light level is acceptable. In order for the space to glow from within during the evening hours, illumination of surfaces was an important design criterion. The wood panels were highlighted using spot lights will allows them to be quite visible from outside at night.

Because of the high ceiling, some HID fixtures were necessary to allow sufficient light to strike the floor. Because of this, the ability to dim the entire space was lost but those luminaires can simply be switched off at certain times.


Figure 1.2.6 - Illuminance Contours

| Atrium Illuminance Data (fc) |  |
| :---: | :---: |
| Floor |  |
| Average | 12.07 |
| Max | 22.6 |
| Min | 3 |
| Avg/Min | 4.02 |
| $\mathrm{Max} / \mathrm{Min}$ | 7.53 |

Table 1.2.4 - Atrium Illuminance Data
The target illuminance on the atrium floor was reach with the proposed lighting design.

## Renderings



Image 1.2.1 - Atrium Pseudo Color Rendering


Image 1.2.2 - Raytraced image looking into atrium


Image 1.2.3 - Raytraced image inside atrium

## Conclusion

The lighting design for the atrium allows it to be used as a transition space or a place to relax. The low light levels provide a nice atmosphere to be in while allowing people passing through to get to their destination easily. The ends of the space are bright which will draw pedestrians through the space.

From the outside, the atrium does what it was designed to do: grab peoples' attention. The illuminated surfaces really glow at night from the outside which makes the space interesting and inviting.

## ATRIUM DAYLIGHT STUDY

## Introduction

It will be seen later in this report that the glass in the atrium was studied as a way to reduce heating and cooling loads. After that was completed, it became clear that it was necessary to see how the new glazing would affect the direct daylight entering the space at various times of the year. The atrium faces south-east which would raises a concern about sunlight penetration into the space at certain times of the year. The daylight study focuses strictly on direct daylight (i.e. clear sky). The days that were studied were March 20, June 21, September 21, and December 21. Each day was studied at $9 \mathrm{am}, 12 \mathrm{pm}$, and 3 pm .

The study focuses on direct sunlight entering the space and how that affects illuminance levels. Also, the glare in the space was looked at in a qualitative manner.

| Original Atrium Glazing |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Viracon No. | Description | Vis. Light | Transmitt <br> Solar <br> Energy | ance <br> Ultra- <br> Violet | Vis. Light-Ext. | Reflectance <br> Vis. <br> Light-Int. | Solar Energy | ASHRAE <br> Winter Night | E U-Value Summer Day | Shading Coeff. | Relative <br> Heat Gain | Area (SF) |
| VRE 1-38 | Solarscreen (clear) | 36\% | 19\% | 12\% | 44\% | 21\% | 46\% | 0.25 | 0.21 | 0.26 | 55 | 880 |
| VRE 1-38 Frit | Silkscreen (dots) | 25\% | 13\% | 7\% | 40\% | 25\% | 13\% | 0.30 | 0.26 | 0.21 | 46 | 2592 |
| VE 1-2M w/ Metallic Opac | Spandrel | 0\% | Not Avail. | Not Avail. | Not Avail. | Not Avail. | Not Avail. | 0.07 | 0.07 | N/A | Not Avail. | 674 |
| New Atrium Glazing |  |  |  |  |  |  |  |  |  |  |  |  |
| Viracon No. | Description | Vis. Light | Transmitta <br> Solar <br> Energy | ance <br> Ultra- <br> Violet | Reflectance |  | Solar Energy | ASHRAE U-Value Winter Summer |  | Shading Coeff. | Relative <br> Heat Gain | Area (SF) |
| VRE 7-38 | Solarscreen (clear) | 28\% | 11\% | 9\% | 28\% | 21\% | 14\% | 0.25 | 0.21 | 0.19 | 41 | 880 |
| VRE 1-38 Frit | Silkscreen (dots) | 19\% | 8\% | 5\% | 26\% | 24\% | 13\% | 0.30 | 0.26 | 0.17 | 37 | 1795 |
| VE 1-2M w/ Metallic Opac | Spandrel | 0\% | Not Avail. | Not Avail. | Not Avail. | Not Avail. | Not Avail. | 0.07 | 0.07 | N/A | Not Avail. | 1471 |

Table 1.3.1 - Atrium Glazing Comparison
*See Appendix E for Glazing Cutsheets

Original Glazing - March


Images 1.3.1,2,3 - March 20 ${ }^{\text {th }}$ Daylighting w/ Original Glazing

| Original Glazing - March 20th <br> Illuminance Data |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | :---: |
| 0900 |  |  | 1200 |  | 1500 |  |
| Average | 663.73 | Average | 788.96 | Average | 36.92 |  |
| Maximum | 1952.00 | Maximum | 2845.00 | Maximum | 4639.00 |  |
| Minimum | 8.70 | Minimum | 8.20 | Minimum | 0.20 |  |
| Avg/Min | 76.29 | Avg/Min | 96.21 | Avg/Min | 184.60 |  |
| Max/Min | 224.32 | Max/Min | 346.93 | Max/Min | 23194.00 |  |

Table 1.3.2 - March Original Glazing Illuminance Data

## New Glazing - March



Images 1.3.4,5,6 - March 20 ${ }^{\text {th }}$ Daylighting w/ New Glazing

| New Glazing - March 20th <br> Illuminance Data |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: |
| 0900 |  | 1200 |  | 1500 |  |
| Average | 456.24 | Average | 506.98 | Average | 26.40 |
| Maximum | 1491.00 | Maximum | 2179.00 | Maximum | 4625.00 |
| Minimum | 6.50 | Minimum | 3.90 | Minimum | 0.10 |
| Avg/Min | 70.22 | Avg/Min | 129.99 | Avg/Min | 264.00 |
| Max/Min | 229.38 | Max/Min | 558.72 | Max/Min | 46248.00 |

Table 1.3.3 - March New Glazing Illuminance Data

Original Glazing - June


Images 1.3.7,8,9 - June $2^{\text {st }}$ Daylighting w/ Original Glazing

| Original Glazing - June 21st <br> Illuminance Data |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: |
| 0900 |  | 1200 |  | 1500 |  |
| Average | 296.00 | Average | 182.25 | Average | 30.29 |
| Maximum | 2432.00 | Maximum | 8884.00 | Maximum | 88.70 |
| Minimum | 0.60 | Minimum | 0.10 | Minimum | 0.10 |
| Avg/Min | 493.33 | Avg/Min | 1823.00 | Avg/Min | 302.90 |
| Max/Min | 4053.00 | Max/Min | 88839.00 | Max/Min | 887.00 |

Table 1.3.4 - June Original Glazing Illuminance Data

New Glazing - June


Images 1.3.10,11,12 - June 21 ${ }^{\text {st }}$ Daylighting w/ New Glazing

| New Glazing - June 21st <br> Illuminance Data |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: |
| 0900 |  | 1200 |  | 1500 |  |
| Average | 190.68 | Average | 105.35 | Average | 21.61 |
| Maximum | 1871.00 | Maximum | 8871.00 | Maximum | 68.20 |
| Minimum | 0.50 | Minimum | 0.10 | Minimum | 0.10 |
| Avg/Min | 381.36 | Avg/Min | 1054.00 | Avg/Min | 216.10 |
| Max/Min | 3743.00 | Max/Min | 88711.00 | Max/Min | 682.00 |

Table 1.3.5 - June New Glazing Illuminance Data

Original Glazing - September


Images 1.3.13,14,15 - September $21{ }^{\text {st }}$ Daylighting w/ Original Glazing

| Original Glazing - September 21st     <br> Illuminance Data     |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | :---: |
| 0900 |  |  | 1200 |  | 1500 |  |
| Average | 794.90 | Average | 682.48 | Average | 33.54 |  |
| Maximum | 2052.00 | Maximum | 2856.00 | Maximum | 4209.00 |  |
| Minimum | 24.70 | Minimum | 6.60 | Minimum | 0.10 |  |
| Avg/Min | 32.18 | Avg/Min | 103.41 | Avg/Min | 335.40 |  |
| Max/Min | 83.06 | Max/Min | 432.67 | Max/Min | 42085.00 |  |

Table 1.3.6 - September Original Glazing Illuminance Data

New Glazing - September


Images 1.3.16,17,18 - September 21 ${ }^{\text {st }}$ Daylighting w/ New Glazing

| New Glazing - September 21st <br> Illuminance Data |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: |
| 0900 |  | 1200 |  | 1500 |  |
| Average | 526.58 | Average | 442.46 | Average | 24.41 |
| Maximum | 1562.00 | Maximum | 2193.00 | Maximum | 4202.00 |
| Minimum | 3.20 | Minimum | 3.80 | Minimum | 0.10 |
| Avg/Min | 164.56 | Avg/Min | 116.44 | Avg/Min | 244.10 |
| Max/Min | 488.09 | Max/Min | 577.05 | Max/Min | 42022.00 |

Table 1.3.7 - September New Glazing Illuminance Data

Original Glazing - December


Images 1.3.19,20,21 - December $21^{\text {st }}$ Daylighting w/ Original Glazing

| Original <br> Illazing - December 21st <br> Illuminance Data |  |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | :---: |
| 0900 |  |  | 1200 |  | 1500 |  |
| Average | 382.62 | Average | 766.31 | Average | 38.70 |  |
| Maximum | 818.00 | Maximum | 1725.00 | Maximum | 506.00 |  |
| Minimum | 10.00 | Minimum | 25.20 | Minimum | 0.20 |  |
| Avg/Min | 38.26 | Avg/Min | 30.41 | Avg/Min | 193.50 |  |
| Max/Min | 81.76 | Max/Min | 68.47 | Max/Min | 2530.00 |  |

Table 1.3.8 - December Original Glazing Illuminance Data

## New Glazing - December



Images 1.3.19,20,21 - December $2^{\text {st }}$ Daylighting w/ New Glazing

| New Glazing - December 21st <br> Illuminance Data |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: |
| 0900 | 1200 |  | 1500 |  |  |
| Average | 286.23 | Average | 550.30 | Average | 27.27 |
| Maximum | 618.00 | Maximum | 1320.00 | Maximum | 387.00 |
| Minimum | 7.50 | Minimum | 16.00 | Minimum | 0.20 |
| Avg/Min | 38.16 | Avg/Min | 34.39 | Avg/Min | 136.20 |
| Max/Min | 82.35 | Max/Min | 82.53 | Max/Min | 1937.00 |

Table 1.3.8 - December New Glazing Illuminance Data

## Daylight Analysis

In each case, the new glazing system lowers the illuminance level on the floor of the atrium. Also, in each case, the new glass prevents the direct sunlight from penetrating as deeply into the space as it did with the original glazing system. Looking at the images of the original glazing versus the new glazing, one can imagine that the new glazing system would make the atrium more comfortable to sit in. Both the lower illuminance levels and shallower penetration would result in a less harshly daylight lit space.

Also, with the original glazing, particularly in December, the direct sunlight reaches the coffee bar and seating areas which are directed adjacent to the atrium. The new glazing system prevents that which would make for a more comfortable experience for the people who are in the rooms next to the atrium.

Overall, the new glazing system performs better when it comes to daylighting. Later in this report, mechanical loading is addressed along with cost analysis of the new glazing system. At that time, this report will weigh the cost versus benefits of this new glazing system.

## 135-SEAT CLASSROOM

## Introduction

The 135 -seat classroom is the largest lecture space in the law school. The space is laid out in a "Ushape" which allows for a lot of seating without forcing the back row to be very far from the front. The seating in the space is tiered to allow for clean sight lines. In the front of the space there is a large presentation area equipped with a retractable projection screen and permanent white boards. This space will provide several different functions for the law students. The functions include: lecturing, presenting, classroom discussion and reading tasks such as exam taking.

Space Layout


Figure 1.4.1 - 135-Seat Classroom Floor Plan


Figure 1.4.2 - 135-Seat Classroom Front Elevation/Section


Figure 1.4.3-135-Seat Classroom North Elevation/Section


Figure 1.4.4-135-Seat Classroom Back Elevation/Section

## Architectural Finishes

Floor


Carpet
Blue/Gray
Reflectance: 33\%

Walls


Painted Gyp Board
Heron White
Finish: Matte
Reflectance: 85\%


Acoustical Fabric
Tan
Reflectance: 54\%


Wood Framing
Dark Stain
Reflectance: 14\%

Ceiling


Painted Gyp Board
Heron White
Finish: Matte
Reflectance: 85\%


Acoustical Ceiling Tile
White
Reflectance: 89\%

Desks
Wood
Dark Stain
Reflectance: 14\%

## Design Goals

The goal for the lighting system in the large classroom is to provide a functional space that is flexible and user friendly. The lighting system should provide the required illuminance values, allow each task to be completed comfortably, and be able to be changed by any user desiring to do so. Aside from meeting the required lighting levels, the system should be attractive and add to the excellence of the law school.

## Target Illuminance Values

Work Plane (Desks) - 30 fc (horizontal)
White Board - 5 fc (vertical)

## Design Criteria

- Color Appearance (Very Important)

Color appearance is very important in this space because of the amount of wood that is present in the architecture. In order to show off the sharpness of the medium-toned wood, a high CRI is needed.

- Daylighting Integration and Control (Not Important)

This space has no glazing and therefore no daylight.

- Direct Glare (Very Important)

This space is a reading intensive space and therefore it is important that the students can read comfortably without having to strain their eyes as a result of direct glare. Also, when the students are looking from the tiered seats, if the intensity of light from high angles is too high, the students will again be straining to shield their eyes while they gaze upon the instructor in the front of the room.

- Flicker (Not Applicable)

This problem is mostly applicable to HID sources and older fluorescent sources. As this is new construction, new fluorescent technology does not present a problem in this area.

- Light Distribution on Surfaces (Important)

Again, because of the amount of wood in the space, light distribution on those wood surfaces is important. Also, the white boards in the front of the room will require light to be distributed evenly to allow all students in the room the opportunity to read the boards easily.

- Uniform Light Distribution on Task Plane (Important)

This criterion is important because of the amount of work that takes place on the desk tops. These tasks include taking notes, taking exams, reading from text books and perhaps typing on a laptop.

- Modeling of Faces (Important)

This is somewhat important in the entire room but mostly important in the front of the room where the instructor will be standing. The students will need to be able to see the instructor and it is much more pleasant to see a face that is illuminated from the front as opposed to straight down because of the strong shadows strong downlight cast on the face.

- Points of Interest (Somewhat Important)

This room does not have many points of interest, but it may be possible to accent the acoustical panels on the wall since they are a darker color than the adjacent walls and would allow yet another way to bring the wood in the room out. Lighting these in a strategic manner could add to the overall look of the room.

- Surface Characteristics (Important)

This will be important on surfaces with texture. Accenting the acoustical panels will add an interesting element while breaking up the painted wall.

- System Control and Flexibility (Important)

This is important as this room has the potential to be used in multiple ways. The room will most often be used for lectures. These lectures could be based around the whiteboard which will require a high level to allow all occupants to read what has been written. Lectures can also be presented with the help of projector, and in this case the lighting levels will have to be reduced to allow for the audience to see the screen. Lastly, if the lecture takes the form of a demonstration, different light levels may be desired than the other two scenarios. Automatic shut-off will be provided using occupancy sensors to comply with ASHRAE 90.1.

- VDT Use (Somewhat Important)

This space has potential for laptop use which will require a limitation of high light angles.

Luminaire Schedule

| Image | Tag | Description | Volt | Manuf. | Cat. No. |  | Lamp |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | F1 | Direct/Indirect <br> Pendant | 277 | Zumtobel | AQ-2545-4-T-DS-U-C1 | Type |  |

Table 1.4.1 - 135-Seat Classroom Luminaire Schedule

Lighting Layout


Figure 1.4.5 - 135-Seat Classroom Lighting Plan

## Controls

The controls in the 135 -seat classroom will consist of occupancy sensors in order to meet ASHRAE 90.1 standard for automatic shut-off. The lighting will be controlled by a scene controller such as Lutron's Grafik Eye 3000. Scenes will be set based on use of the space. Please refer to electric depth, page 94 for details on classroom controls.

## Light Loss Factors

| Tag | Descr. | Cat. | Class | Dirt | Cleaning | LDD | RSDD | LLD | BF | LLF |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- |
| F1 | Pendant <br> Lighting | VI | Semi- <br> Indirect | Clean | 12 mos. | 0.85 | 0.92 | 0.92 | 1.00 | $\mathbf{0 . 7 2}$ |
| F2 | Recessed <br> Downlight | IV | Direct | Clean | 12 mos. | 0.88 | 0.98 | 0.84 | 0.95 | $\mathbf{0 . 6 9}$ |
| F3 | Recessed <br> Downlight <br> WW | IV | Direct | Clean | 12 mos. |  |  |  |  |  |
| F4 | Board Light | V | Direct | Clean | 12 mos. | 0.88 | 0.98 | 0.92 | 1.05 | $\mathbf{0 . 8 3}$ |
| F5 | Cove Light | V | Indirect | Clean | 12 mos. | 0.88 | 0.92 | 0.92 | 1.00 | $\mathbf{0 . 7 4}$ |

Table 1.4.2 - 135-Seat Classroom Light Loss Factors
Power Density

| Room: | Classroom | Desired WP FC: | 30 |  |
| :---: | :---: | :---: | :---: | :---: |
| Square Footage: | 3085 | Ashrae Allow: |  |  |
| Total Watts Allowed: | 4319 |  |  |  |
| TAG | DESCRIPTION | WATTS | NO. USED | TOTAL WATTS |
| F1 | Pendant Lighting | 68 | 24 | 1632 |
| F2 | Recessed Downlight | 36 | 23 | 828 |
| F3 | Recessed Downlight Wall Wash | 46 | 14 | 644 |
| F4 | Board Light | 34 | 8 | 272 |
| F5 | Cove Light | 34 | 7 | 238 |
| 11 | Track Lighting | 100 | 7 | 700 |
| TOTAL ROOM WATTS: ROOM WATTS REMAINING: | $\begin{aligned} & 4314 \\ & 5 \end{aligned}$ | Power Density: 1.40 <br> Actual to Allowed: $99.88 \%$ |  |  |

Table 1.4.3 - 135-Seat Classroom Power Density
The 135-Seat Classroom uses almost one hundred percent of its allotted watts for lighting. This room serves many functions and has multiple lighting systems including incandescent track lighting which pushes the power density up. The use of fluorescent fixtures for the other sources however, keeps the power density at an acceptable level. Many of the fixtures will either be dimmed or switched off depending on the preset scene so this space will not always be using 1.4 watts per square foot.

## Design Performance

The lighting system that was designed for the classroom is one that is subtle yet interesting. Architecturally attractive indirect/direct luminaires provide the majority of the general lighting in the space. Recessed downlights are used in conjunction with the pendants to meet the necessary task plane light levels. Cove lighting is used to break the ceiling and add another interesting element to the architecture. The acoustical panels that are located on the perimeter are accented using recessed wall wash fixtures. The presentation area is lighted using track fixtures to illuminate the face of the presenter while fluorescent fixtures are used to illuminate the white board.


Figure 1.4.6 - 135-Seat Classroom Illuminance Contours

| 135-Seat Class | ance Data (fc) | 135-Seat Class | ance Data (fc) |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| Average | 32.32 | Average | 36.00 |
| Max | 38.90 | Max | 45.30 |
| Min | 24.30 | Min | 19.50 |
| Avg/Min | 1.33 | Avg/Min | 1.85 |
| Max/Min | 1.60 | Max/Min | 2.32 |
| Table 1.4.4 - Classroom Row 1 Illum. Data |  | Table 1.4.5 - Classroom Row 2 Illum. Data |  |
| 135-Seat Classroom Illuminance Data (fc) |  | 135-Seat Classroom Illuminance Data (fc) |  |
| Desks: Row 3 |  | Desks: Row 4 |  |
| Average | 36.18 | Average | 33.94 |
| Max | 46.80 | Max | 45.80 |
| Min | 20.20 | Min | 19.10 |
| Avg/Min | 1.79 | Avg/Min | 1.78 |
| Max/Min | 2.32 | Max/Min | 2.40 |
| Table 1.4.6 - Classroom Row 3 Illum. Data |  | Table 1.4.7 - Classroom Row 4 Illum. Data |  |


| 135-Seat Classroom Illuminance Data (fc) |  | 135-Seat Class | ance Data (fc) |
| :---: | :---: | :---: | :---: |
| Desks: Row 5 |  | Desks: Row 6 |  |
| Average | 32.79 | Average | 26.62 |
| Max | 55.00 | Max | 45.50 |
| Min | 13.90 | Min | 13.60 |
| Avg/Min | 2.36 | Avg/Min | 1.96 |
| Max/Min | 3.96 | Max/Min | 3.35 |
| Table 1.4.8 - Classroom Row 5 Illum. Data |  | Table 1.4.9 - Classroom Row 6 Illum. Data |  |
| 135-Seat Classroom Illuminance Data (fc) |  |  |  |
|  | White Board |  |  |
|  | Average | 47.65 |  |
|  | Max | 100.00 |  |
|  | Min | 21.00 |  |
|  | Avg/Min | 2.27 |  |
|  | Max/Min | 4.84 |  |
| Table 1.4.10 - Classroom White Board Illum. Data |  |  |  |

A few of the previous reports are slightly misleading. Each calculation plane extends from the front edge of the desk back to the next level (whether that is another desk or a wall.) Because of this, some of the minimum foot-candle values are skewed slightly low. Also, the white board calculation was performed with the luminaires at full output. In reality, these luminaires have dimming ballasts and would be dimmed to an appropriate level based on the needs of the users. The reason the illuminance on the surface is so high is in order to have uniform lighting, the luminaires are place side by side for the length of the board.

## Renderings



Image 1.4.1 - 135-Seat Classroom Pseudo Color Rendering


Image 1.4.2 - 135-Seat Classroom Lecturer's View


Image 1.4.3 - 135-Seat Classroom Student's View


Image 1.4.4 - 135-Seat Classroom Raytraced Rendering

## Conclusion

The lighting system for the classroom successfully provided necessary light levels. The desks that are partially under the low ceiling are not as uniformly lighted as the others because parts are being lighted with a different type of lighting. For the most part however, the lighting levels are fairly uniform. The accenting on the acoustical panels provides some very nice visual interest on the perimeter while the cove makes for an interesting element on the ceiling. The flexibility of this space makes it easy to change the lighting based on the task that is being completed.

## MOOT COURTROOM

## Introduction

The moot courtroom is a functional courtroom that will be used for mock trial proceedings. The space consists of tiered seating, a presentation area, a judges' bench, a jury box, a witness stand and counselors' tables. The space, at times, will be used much like a classroom. There will be lectures, presentations, classroom discussion and exam taking. Students have the unique opportunity of experiencing a true courtroom setting while learning the ways of a trial lawyer. The lighting in this space will be flexible to allow for all tasks to be completed successfully as well as to enhance the many interesting architectural elements of the courtroom.

## Space Layout



Figure 1.5.1 - Moot Court Floor Plan


Figure 1.5.2 - Moot Court Front Elevation/Section


Figure 1.5.3 - Moot Court Rear Elevation/Section


Figure 1.5.4 - Moot Court North Elevation/Section


Figure 1.5.5 - Moot Court South Elevation

## Architectural Finishes

Floor


Carpet
Blue/Gray
Reflectance: 33\%

Walls


Painted Gyp Board
Heron White
Finish: Matte
Reflectance: 85\%


Acoustical Fabric
Tan
Reflectance: 54\%


Wood Framing
Dark Stain
Reflectance: 14\%


Wood Paneling
Dark Stain
Reflectance: 14\%

## Ceiling



Painted Gyp Board

Heron White
Finish: Matte
Reflectance: 85\%


Acoustical Ceiling Tile
White
Reflectance: 89\%


Painted Gyp Board
Simply White
Finish: Matte
Reflectance: 80\%

## Design Goals

The main goal in the courtroom is to provide a learning space that can meet all the demands of the users. The space must be able to be used as a typical classroom as well as a courtroom. The courtroom setting should be as realistic as possible. The controls in the space should allow the users to change scenes quickly and easily.

## Target Illuminance Levels

Work Plane (Desks) - 30 fc (horizontal)

## Design Criteria

- Appearance of Space and Luminaires (Very Important)

This space is one of the most important spaces in the law school because this is where the mock proceedings take place. This space needs to be every bit as impressive and perhaps intimidating as a normal courtroom. The appearance of the space and the luminaires needs to show the law students just how impressive a space like this can be so they are ready for it when they experience the real thing.

- Color Appearance (Very Important)

Like in the classroom, this is so important because of the amount of wood in the space. This space has even more wood that the classroom so the color appearance of the space is critical if the wood is going to stand out in the way the architect intended.

- Daylighting Integration and Control (Not Important)

There is no daylighting in this space.

- Direct Glare (Important)

The audience will be seated higher toward the back of the room, so if the light from high angles is very intense they will have a difficult time looking past that toward the proceedings in the front of the room. In a real court room, a jury could be there for many days at a time, and comfortable lighting is critical if one expects them to pay attention and be comfortable for the time they are there.

- Flicker (Not Applicable)

This problem is mostly applicable to HID sources and older fluorescent sources. As this is new construction, new fluorescent technology does not present a problem in this area.

- Light Distribution on Surfaces (Important)

The wood in this room demands attention and distributing light on those surfaces is a way to give the wood the attention it deserves.

- Uniform Light Distribution on Task Plane (Important)

This space is not a very reading intensive space other than in the front of the room. The judge will be reading and the prosecution and defense will surely be reading, while the audience will often times just be observing. However, the audience will need to be able to read when this space is being used as a classroom and therefore the task plane distribution can be addressed by the different scenes that the control panel provides.

- Modeling of Faces (Important)

This is important in the area of the courtroom where the proceedings or lecture will be taking place. The jury and audience need to see the judges' and witness' faces well. On the other hand, the jury and judge also need to be able to see the counselors' and the defendant's faces well so the front of the space will need to be illuminated well vertically from the sides and not from directly forward.

- Points of Interest (Important)

In this courtroom the biggest point of interest will be the bench and the logo behind it. This is an area that you want everyone looking. Illuminating this area effectively is very important.

- Surface Characteristics (Important)

This again relates mostly to the amount of wood in the room. The wood throughout the room certainly needs to be lighted, but the wood on the front wall now has the opportunity to bring even more visual interest to the space so the illumination of that needs to be addressed.

- System Control and Flexibility (Very Important)

This is a space that will serve as an instructional area in multiple ways. A typical classroom setting has to be provided, along with a traditional courtroom environment. There are many high quality materials in this space so the space needs to be able to be controlled to a high quality lighting design at times as well.

## Luminaire Schedule

| Image | Tag | Description | Volt | Manuf. | Cat. No. | Lamp |  | Mounting |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | No. | Type |  |
|  | F1 | Direct/Indirect Pendant | 277 | Zumtobel | AQ-2545-4-T-DS-U-C1 | 2 | $\begin{aligned} & \text { 28W } \\ & \text { T5 } \end{aligned}$ | Pendant |
|  | F3 | Recessed Downlight WW | 277 | Zumtobel | S5D-U-7309HW-C | 1 | $\begin{aligned} & \hline 42 \mathrm{~W} \\ & \mathrm{CFL} \end{aligned}$ | Recessed |
|  | F5 | Cove Light | 277 | Lightolier | CL-1-4-T5-2 | 1 | $\begin{aligned} & 28 \mathrm{~W} \\ & \text { T5 } \end{aligned}$ | Surface |
| $\square$ | F6 | Recessed Parabolic Downlight | 277 | Zumtobel | S5D-U-7703T-C | 2 | $\begin{aligned} & 18 \mathrm{~W} \\ & \text { CFL } \end{aligned}$ | Recessed |
|  | F7 | Recessed Linear Fluorescent | 277 | Se'lux | $\begin{aligned} & \text { M6R2-1T5-SD-SH-004- } \\ & \text { WH-277 } \end{aligned}$ | 1 | $\begin{aligned} & \text { 28W } \\ & \text { T5 } \end{aligned}$ | Recessed |
|  | F8 | Recessed <br> Linear <br> Fluorescent WW | 277 | Focal <br> Point | $\begin{aligned} & \text { FAVA-NS-1T5-1C- } \\ & \text { 277-S-F } \end{aligned}$ | 1 | $\begin{aligned} & \text { 28W } \\ & \text { T5 } \end{aligned}$ | Recessed |

Table 1.5.1 - Moot Court Luminaire Schedule

## Lighting Layout



Figure 1.5.6 - Moot Court Lighting Plan

## Controls

The controls in the moot court will consist of occupancy sensors in order to meet ASHRAE 90.1 standard for automatic shut-off. The lighting will be controlled by a scene controller such as Lutron's Grafik Eye 3000. Scenes will be set based on use of the space. Please refer to electric depth, page 103 for details on classroom controls.

## Light Loss Factors

| Tag | Descr. | Cat. | Class | Dirt | Cleaning | LDD | RSDD | LLD | BF | LLF |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F1 | Direct/Indirect Pendant | VI | Semiindirect | Clean | 12 mos . | 0.85 | 0.92 | 0.92 | 1.00 | 0.72 |
| F3 | Recessed Downlight WW | IV | Direct | Clean | 12 mos. | 0.88 | 0.98 | 0.84 | 0.95 | 0.69 |
| F5 | Cove Light | V | Indirect | Clean | 12 mos. | 0.88 | 0.92 | 0.92 | 1.00 | 0.74 |
| F6 | Recessed <br> Parabolic <br> Downlight | IV | Direct | Clean | 12 mos. | 0.88 | 0.98 | 0.81 | 0.95 | 0.66 |
| F7 | Recessed Linear Fluorescent | V | Direct | Clean | 12 mos . | 0.88 | 0.97 | 0.92 | 1.00 | 0.79 |
| F8 | Recessed Linear Fluorescent WW | V | Direct | Clean | 12 mos . | 0.88 | 0.97 | 0.92 | 1.00 | 0.79 |

Table 1.5.2 - Moot Court Light Loss Factors
Power Density

| Room: | Moot Courtroom | Desired WP FC: 30 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Square Footage: | 2134 | Ashrae Allow: 1.9 |  |  |
| Total Watts Allowed: | 4054.6 |  |  |  |
| TAG | DESCRIPTION | WATTS | NO. USED | TOTAL WATTS |
| F1 | Pendant Lighting | 68 | 8 | 544 |
| F3 | Recessed Downlight Wall Wash | 46 | 14 | 644 |
| F5 | Cove Light | 34 | 7 | 238 |
| F6 | Recessed Downlight Parabolic | 41 | 21 | 861 |
| F7 | Recessed Linear Fluorescent | 34 | 6 | 204 |
| F8 | Recessed Linear Fluor. Wall Wash | 34 | 4 | 136 |
| 11 | Track Lighting | 100 | 7 | 700 |
| TOTAL ROOM WATTS: ROOM WATTS REMAINING: | $\begin{aligned} & 3327 \\ & 727.6 \\ & \hline \end{aligned}$ | Power Density: Actual to Allowed: | $\begin{array}{r} 1.56 \\ 82.05 \% \\ \hline \end{array}$ |  |

## Table 1.5.3 - Moot Court Power Density

The courtroom performs very well on the energy side. Only 82 percent of the watts allowed by ASHRAE are being used in the lighting design. This is a space that will help the law school save energy or meet the ASHRAE requirement because of its low energy consumption. The incandescent spots that are used to illuminate the judges' and witnesses' faces are the reason the power density is as high as it is. Without those, the power density would be around $65 \%$ of what is allowed by ASHRAE. Incandescents perform very well for facial rendering and it was determined that that fact justified using the inefficient incandescent sources.

## Design Performance

The lighting in the courtroom is similar to that of the classroom and performs much the same way. The desks are relatively uniform, the walls are accented and provide a nice pattern and there is some interest on the ceiling. The courtroom differs greatly from the classroom at the front of the space. This space is lighted with low profile recessed linear strips and incandescent spot lights. The judges’ bench has an average of 20 fc which seems low but because this will be used much less often than the rest of the space, individual task lighting would add a nice touch and increase the illuminance on the judges' bench. Many courtroom images show a judge looking at evidence under a task-light. This will help add to the realism. The architecture in the front of the room is the main focal point and is lighted accordingly.


Figure 1.5.7 - Moot Court Illuminance Contours


Table 1.5.8 - Moot Court Judges' Bench Illum. Data
The uniformity of this lighting system is better than that of the classroom. The reason for this is the high ceilings. The light has the ability to spread out more and hits the plane more evenly.

## Renderings



Image 1.5.1 - Moot Court Pseudo Color Rendering


Image 1.5.2 - Moot Court View from Presentation Area


Image 1.5.3 - Moot Court Student View


## Image 1.5.4 - Moot Court Raytraced Student View

## Conclusion

The lighting system in the moot court successfully provides sufficient light levels and does so in a uniform fashion. The lighting system also does a good job of providing illumination to the judges' and witnesses' faces while still accenting the architecture in the front of the room. The panels on the side wall once again provide some perimeter interest while the different ceiling heights provide visual interest above. The flexibility of the room will allow it to be used as a classroom, lecture hall, courtroom or whatever else is needed.

## Electrical Depth

## ELECTRICAL COORDINATION OF LIGHTING DESIGN

## Introduction

The electrical coordination of the four lighting designs will be explored in this section. For each lighting space, the existing lighting panelboards are evaluated and redesigned in accordance with the lighting changes. Each original panelboard that is affected by the new lighting designs is shown with the affected circuits highlighted in gray. A panelboard worksheet will be provided which aided in the resizing of the panelboard. A feeder worksheet and an updated panelboard will be shown as well.

A few of the existing panels are not sized correctly according to the panelboard worksheets. This may because the correct loads were never entered into the spreadsheet or the correct sizing information was not entered into the spreadsheets until the final release. I did not resize the original panels to meet the demand load; my redesigned panelboards however will be resized to ensure they can carry the necessary load.

Feeder and conduit sizes for each revised panelboard are determined using NEC 2005.

## Courtyard

The courtyard lighting redesign was meant to be subtle and mostly serve the purpose of allowing people to get from the building to the parking lot or vice versa. The atrium, which is the cornerstone of the law school's lighting design, lies directly beyond the courtyard. Because of this the courtyard was designed to allow the atrium to make the statement that was meant to be made.

The panels that will be affected by the courtyard lighting redesign are as follows: LP-1N which is located in Electric Room 188 on the first floor, LP-3N which is located in Electric Room 366 on the third floor and LP-BS which is located in B02 in the sub-basement.

The control system for the courtyard will be an existing lighting control panel. The luminaires in the courtyard will operate on a time clock. All luminaires will be switched on in the evening and switch off the next morning. This system will play an important role in saving energy.

The following table outlines the overprotection, feeder and conduit information for the existing panels for the courtyard.

| Affected Courtyard Panels |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Feeder |  |  |  |  |
| Panelboard | Breaker | Sets | Phase | Neutral | Ground | Conduit |
| LP-1N | $400 \mathrm{~A}, 3 \mathrm{P}$ | 2 | $3 \# 3 / 0$ | $1 \# 3 / 0$ | $1 \# 6$ | $(2) 2^{\prime \prime}$ |
| LP-3N | $150 \mathrm{~A}, 3 \mathrm{P}$ | 1 | $3 \# 1 / 0$ | $1 \# 1 / 0$ | $1 \# 6$ | $2^{\prime \prime}$ |
| LP-BS | $225 A, 3 P$ | 1 | $3 \# 4 / 0$ | $1 \# 4 / 0$ | $1 \# 4$ | $2-1 / 2^{\prime \prime}$ |

Table 2.1.1 - Courtyard Affected Panelboard Information


Figure 2.1.1 - Courtyard Electrical Plan
*Please refer to Appendix B for full size plan

| Original LCP-1 |  |  |
| :---: | :---: | :---: |
| Relay | Circuit | Time Schedule |
| 1 | LP-1N-8 | 8AM-6PM |
| 2 | LP-1N-9 | 7AM-10PM |
| 3 | LP-1N-12 | 7AM-10PM |
| 4 | LP-1S-15 | 7AM-10PM |
| 5 | LP-1S-20 | PHOTOCELL |
| 6 | ELP-1N-S | PHOTOCELL |
| 7 | LP-BS-9 | PHOTOCELL |
| 8 | LP-1N-14 | PHOTOCELL |

Figure 2.1.2 - Existing Control Panel Schedule

| Revised LCP-1 |  |  |
| :---: | :--- | :--- |
| Relay | Circuit | Time <br> Schedule |
| 1 | LP-1N-13 | 6PM-6AM |
| 2 | LP1N-15 | 6PM-6AM |
| 3 | LP-1N-17 | 6PM-6AM |
| 4 | LP-3N-22 | 6PM-6AM |
| 5 | LP-BS-11 | 6PM-6AM |
| 6 | SPARE |  |
| 7 | SPARE |  |
| 8 | SPARE |  |

Figure 2.1.3 - Existing Control Panel Schedule


Figure 2.1.4 - LP-1N Existing Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.1.5 - LP-1N Panelboard Worksheet
Jason Greer I Villanova University: School of Law

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: LP-1N | EQUIP. GND. BUS: |  |  |  |  | VOLTAGE: |  |  |  | $480 / 277$ VOLT, 3PH, 4W |
| LOCATION: ELEC.RM.(188)-1ST FL. | ISOLATED GND BUS: |  |  |  |  | 200\% | MAIN CIRCUIT BKR: |  |  |  |
| MOUNTING: SURFACE | NEUTRAL BUS: |  |  | 100\% |  |  | $\square$ | MLO: |  |  |
| FED FROM: SWBD 'MDB' |  | A.l.C.: | 42000 |  |  |  |  | BUS RA | IG: | 600 |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-1-3 |  |  | 1 | 3,713 |  |  |  |  |  | RF-1-3 |
|  |  |  |  | 1,275 |  |  | 2 |  |  |  |
|  | 30 | 3 | 3 |  | 3,713 |  |  |  |  |  |
|  |  |  |  |  | 1.275 |  | 4 | 3 | 15 |  |
|  |  |  | 5 |  |  | 3,713 |  |  |  |  |
|  |  |  |  |  |  | 1,275 | 6 |  |  |  |
| LIGHTINGOFFICE SPACE | 20 | 1 | 7 | 4,000 |  |  |  |  |  | LIGHTINGOFFICE CORRIDOR |
|  |  |  |  | 3,176 |  |  | 8 | 1 | 20 |  |
| LIGHTING MAIN CORRIDOR | 20 | 1 | 9 |  | 2,500 |  |  |  |  | LIGHTINGOFFICE SPACE |
|  |  |  |  |  | 1.400 |  | 10 | 1 | 20 |  |
| LIGHTING MAIN SEATING AREA | 20 | 1 | 11 |  |  | 1,400 |  |  |  | LIGHTING CHAPEL |
|  |  |  |  |  |  | 1.800 | 12 | 1 | 20 |  |
| COURTYARD LIGHTING BOLLARDS | 20 | 1 | 13 | 1,786 |  |  |  |  |  | LIGHTINGEXTERIOR READING ROOM |
|  |  |  |  | 1,250 |  |  | 14 | 1 | 20 |  |
| COURTYARD LIGHTING DOWNLIGHTS | 20 | 1 | 15 |  | 374 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 16 | 1 | 20 |  |
| COURTYARD LIGHTING FACADE LIGHTS | 20 | 1 | 17 |  |  | 1,419 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 18 | 1 | 20 |  |
| SPARE | 20 | 1 | 19 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 20 | 1 | 20 |  |
| SPARE | 20 | 1 | 21 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 22 | 1 | 20 |  |
| SPARE | 20 | 1 | 23 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 24 | 1 | 20 |  |
| SPARE | 20 | 1 | 25 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| SPARE | 20 | 1 | 27 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| SPARE | 20 | 1 | 29 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | PANEL 'LP-3N' |
|  |  |  |  | 40.313 |  |  | 32 | 3 | 150 |  |
| SPARE | 20 | 1 | 33 |  |  |  |  |  |  |  |
|  |  |  |  |  | 37.756 |  | 34 |  |  |  |
| LIGHTING CONTROL PANELLCP-1B | 20 | 1 | 35 |  |  | 1,000 |  |  |  |  |
|  |  |  |  |  |  | 36.920 | 36 |  |  |  |
| PANEL 'RP-1NA' (75 KVA XFMR) | 125 | 3 | 37 | 23,511 |  |  |  |  |  | PANEL 'LP-2N' |
|  |  |  |  | 26,681 |  |  | 38 | 3 | 150 |  |
|  |  |  | 39 |  | 18,645 |  |  |  |  |  |
|  |  |  |  |  | 28,445 |  | 40 |  |  |  |
|  |  |  | 41 |  |  | 18,837 |  |  |  |  |
|  |  |  |  |  |  | 25,239 | 42 |  |  |  |
|  | TOTAL VA |  |  | 105,705 | 4.108 | 91.603 | TOTAL KVA |  |  | 291.4 |
|  | TOTAL | AMP/PH |  | 382 | 340 | 331 | TOTAL | MP |  | 351 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 2.1.6 - LP-1N Revised Panelboard Schedule


Figure 2.1.7 - LP-3N Original Panelboard Schedule


Figure 2.1.8 - LP-3N Panelboard Worksheet
Jason Greer I Villanova University: School of Law


Figure 2.1.9 - LP-3N Revised Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EQUIP. GND. BUS: |  |  |  |  |  | VOLTAGE: |  |  | 480/277 VOLT, 3PH, 4W |
| ELEC.RM (B02)-SUB.BSMT |  | ISOLATED GND BUS: |  |  |  | $200 \%$ | MAIN CIRCUIT BKR: |  |  | 225 |
| SURFACE | NEUTRAL BUS: |  |  | 100\% |  |  | $\square$ |  |  |  |
| FED FROM: SWBD 'MDB' |  | A.I.C.: | 65000 |  |  |  |  |  |  |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-1-2 |  |  | 1 | 5,570 |  |  |  |  |  | RF-1-2 |
|  |  |  |  | 2.920 |  |  | 2 |  |  |  |
|  | 40 | 3 | 3 |  | 5,570 |  |  |  |  |  |
|  |  |  |  |  | 2.920 |  | 4 | 3 | 30 |  |
|  |  |  | 5 |  |  | 5,570 |  |  |  |  |
|  |  |  |  |  |  | 2,920 | 6 |  |  |  |
| SPARE | 20 | 1 | 7 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 8 | 1 |  |  |
| SPARE | 20 | 1 | 9 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 10 | 1 | 15 |  |
| SPARE | 20 | 1 | 11 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 12 | 1 |  |  |
| SF-1-2 |  |  | 13 | 7,160 |  |  |  |  |  | RF-1-2 |
|  |  |  |  | 2.920 |  |  | 14 |  |  |  |
|  | 60 | 3 | 15 |  | 7,160 |  |  |  |  |  |
|  |  |  |  |  | 2.920 |  | 16 | 3 | 30 |  |
|  |  |  | 17 |  |  | 7,160 |  |  |  |  |
|  |  |  |  |  |  | 2.920 | 18 |  |  |  |
| SF-2-2 |  |  | 19 | 5,570 |  |  |  |  |  | RF-2-2 |
|  |  |  |  | 2.920 |  |  | 20 |  |  |  |
|  | 40 | 3 | 21 |  | 5,570 |  |  |  |  |  |
|  |  |  |  |  | 2.920 |  | 22 | 3 | 30 |  |
|  |  |  | 23 |  |  | 5,570 |  |  |  |  |
|  |  |  |  |  |  | 2,920 | 24 |  |  |  |
| SF-3-2 |  |  | 25 |  |  |  |  |  |  | RF-3-2 |
|  |  |  |  |  |  |  | 26 |  |  |  |
|  | 20 | 3 | 27 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 28 | 3 | 20 |  |
|  |  |  | 29 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 30 |  |  |  |
| LIGHTING | 20 | 1 | 31 | 2,016 |  |  |  |  |  | LIGHTING DIINING AREA |
|  |  |  |  | 3.500 |  |  | 32 | 1 | 20 |  |
| LIGHTING CONTROL PANELLCP-0B | 20 | 1 | 33 |  | 1,000 |  |  |  |  | LIGHTING SERVING |
|  |  |  |  |  | 2,280 |  | 34 | 1 | 20 |  |
| SPARE | 20 | 1 | 35 |  |  |  |  |  |  | LIGHTINGKTCHEN/SURROUNDING SPACES |
|  |  |  |  |  |  |  | 36 | 1 | 20 |  |
| PANEL 'RP-BS' (30 KVA XFMR) | 125 | 3 | 37 | 25,880 |  |  |  |  |  | LIGHTING LOCKERS |
|  |  |  |  | 1.440 |  |  | 38 | 1 | 20 |  |
|  |  |  | 39 |  | 21,833 |  |  |  |  | $\begin{gathered} \text { L16A,L16B } \\ \text { HAND DRYERS } \end{gathered}$ |
|  |  |  |  |  | 3,048 |  | 40 | 1 | 20 |  |
|  |  |  | 41 |  |  | 21,370 |  |  |  | $\begin{gathered} \text { L09A,B } \\ \text { HAND DRYERS } \end{gathered}$ |
|  |  |  |  |  |  | 3,048 | 42 | 1 | 20 |  |
|  | TOTAL VA |  |  | 59,896 | 55,221 | 51,478 | TOTAL KVA |  |  | 166.6 |
|  | TOTAL AMP/PHASE |  |  | 216 | 199 | 186 | TOTAL AMP |  |  | 200 |

Figure 2.1.10 - LP-3N Original Panelboard Schedule


Figure 2.1.11 - LP-BS Panelboard Worksheet


Figure 2.1.12 - LP-BS Revised Panelboard Schedule

| Courtyard Feeder Sizing Worksheet |  |  |  |
| :--- | ---: | ---: | ---: |
| Panelboard Tag | LP-1N | LP-3N | LP-BS |
| Panelboard Voltage | $480 \mathrm{Y} / 277$ | $480 \mathrm{Y} / 277$ | $480 \mathrm{Y} / 277$ |
| Calculated Design Load (kw) | 346.9 | 134.5 | 225.4 |
| Calculated Design Load (kva) | 346.9 | 134.5 | 225.4 |
| Resultant Power Factor | 1 | 1 | 1 |
| Calculated Design Load (amps) | 417.4 | 161.9 | 271.3 |
| Feeder Protection Size | 450 | 175 | 300 |
| Sets | 2 | 1 | 1 |
| Wire Size |  |  |  |
| Phase | $3 \# 4 / 0$ | $3 \# 3 / 0$ | $3 \# 400 \mathrm{MCM}$ |
| Neutral | $1 \# 4 / 0$ | $1 \# 3 / 0$ | $1 \# 400 \mathrm{MCM}$ |
| Ground | $\# 2$ | $\# 6$ | $\# 4$ |
| Conduit Size | $(2) 2 "$ | $2 "$ | $2-1 / 2 "$ |

Figure 2.1.13 - Courtyard Feeder Sizing Worksheet

## Atrium

The atrium lighting design is meant to serve as the beacon of the law school. With the extensive glazing looking out to the parking lot, everyone will always know where the entrance is. The atrium serves as both a transition space between the two wings of the building and a place to relax. The light levels are low enough to relax but the surfaces are illuminated to a level that allows them to glow outside.

The panels that are affected by the lighting redesign are as follows: LP-1S which is located in Electric Room 119 on the first floor, and LP-2S which is located in Electric Room 219A on the second floor.

This space will be controlled through the use of photo sensors that will be connected to a dimming panel in an electrical room. The HID fixtures will be connected to the same panel but will simply be switched by the photo sensor.

The following table outlines the overprotection, feeder and conduit information for the existing panels for the courtyard.

| Affected Atrium Panels |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Panelboard | Breaker | Feeder |  |  |  |  |
|  |  | Phase | Neutral | Ground | Conduit |  |
|  | 400 A, 3P | 1 | $3 \# 350 M C M$ | $1 \# 350$ MCM | $1 \# 4$ | $3 "$ |
| LP-2S | $225 A, 3 P$ | 1 | $3 \# 4 / 0$ | $1 \# 4 / 0$ | $1 \# 4$ | $2-1 / 2^{\prime \prime}$ |

Figure 2.2.1 - Atrium Affected Panelboard Information


Figure 2.2.2 - Atrium Electrical Plan
*Please see Appendix B for full size plan

| LCD-203 Controller |  |  |
| :--- | :--- | :--- |
| Zone | Circuit | Control |
| A | LP-2S-16 | Photo (Switch) |
| B | LP-1S-19 | Photo (Dim) |
| C | LP-2S-14 | Photo (Dim) |

Figure 2.2.3 - Proposed Photo Sensor Control
*See Appendix C for control specifications


Figure 2.2.4 - LP-1S Existing Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.2.5 - LP-1S Panelboard Worksheet

Jason Greer I Villanova University: School of Law


Figure 2.2.6 - LP-1S Revised Panelboard Schedules


Figure 2.2.7 - LP-2S Original Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.2.8 - LP-2S Panelboard Worksheet


Figure 2.2.9 - LP-2S Revised Panelboard Schedule

| Atrium Feeder Sizing Worksheet |  |  |
| :--- | ---: | ---: |
| Panelboard Tag | LP-1S | LP-2S |
| Panelboard Voltage | $480 \mathrm{Y} / 277$ | $480 \mathrm{Y} / 277$ |
| Calculated Design Load (kw) | 560.5 | 177.4 |
| Calculated Design Load (kva) | 560.5 | 177.4 |
| Resultant Power Factor | 1 | 1 |
| Calculated Design Load (amps) | 674.5 | 213.4 |
| Feeder Protection Size | 700 | 225 |
| Sets | 2 | 1 |
| Wire Size |  |  |
| Phase | $3 \# 400 \mathrm{MCM}$ | $3 \# 4 / 0$ |
| Neutral | $1 \# 400 \mathrm{MCM}$ | $1 \# 4 / 0$ |
| Ground | $\# 1 / 0$ | $\# 4$ |
| Conduit Size | $(2) 2-1 / 2^{\prime \prime}$ | $2 "$ |

Figure 2.2.10 - Atrium Feeder Sizing Worksheet

## 135-Seat Classroom

The 135 -seat classroom is the largest classroom in the law school and is used for everything from lectures, to presentations, to exams and more. The lighting in the space must be flexible to allow for all of those things to take place. The lighting also is designed to bring out the architectural features of the space such as the panels on the walls and the cove in the ceiling.

The panels that are affected by the lighting design are as follows: LP-1S which is located in Electric Room 119A on the first floor and RP-1SA-3 which is also located in 119A.

The controls in the classroom will be a scene controller that is equivalent to Lutron's Grafik Eye 3000. There are four zones in the space, each of which will be controlled according to whichever scene has been selected. Occupancy sensors will also be used to meet ASHRAE 90.1 automatic shutoff criteria.

The following table outlines the overprotection, feeder and conduit information for the existing panels for the courtyard.

| Affected 135-Seat Classroom Panels |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Panelboard | Breaker | Feeder |  |  |  | Conduit |
|  |  | Sets | Phase | Neutral | Ground |  |
| LP-1S | 400A, 3P | 1 | 3\#350MCM | 1\#350 MCM | 1\#4 | 3" |
| RP-1SA-3 | 225A, 3P | 1 | 3\#250MCM | 1\#250MCM | 1\#4 | 2-1/2" |

Figure 2.3.1 - 135-Seat Classroom Affected Panelboard Information


Figure 2.3.2 - 135-Seat Classroom Electrical Plan
*Please see Appendix B for full size plan

| 135-Seat Classroom Scene Matrix |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | :---: |
| Zone |  |  |  |  |  |
| Scene | A | B | C | D |  |
| General <br> Lighting | $100 \%$ | $100 \%$ | $100 \%$ | $100 \%$ |  |
| Lecture | $80 \%$ | $100 \%$ | $50 \%$ | $50 \%$ |  |
| Electronic <br> Presentation | $10 \%$ | $10 \%$ | $80 \%$ | $100 \%$ |  |

Figure 2.3.3. - 135-Seat Classroom Scene Control Matrix
*See Appendix C for control specifications


Figure 2.3.4 - LP-1S Original Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.3.5 - LP-1S Panelboard Worksheet

Jason Greer I Villanova University: School of Law


Figure 2.3.6 - LP-1S Revised Panelboard Schedules

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RP-1SA-3 |  | EQUIP. GND. BUS: |  |  |  | 200\% | VOLTAGE: |  |  | 120/208 VOLT, 3PH, 4W |
| ELEC.RM.(119A)-1ST FL. |  | ISOLATED GND BUS: |  |  |  |  |  | MAIN | RCUIT B | 125 |
| MOUNTING: SURFACE |  | NEUTR | BUS: | 100\% |  |  |  | MLO: | $\square$ |  |
| FED FROM: PANEL 'LP-1S' |  | A.I.C.: | 22000 |  |  |  |  | BUS RA | ING: | 225 |
| LOAD DESCRIPTION | BKR. AMPS | BKR. POLE | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 101 SEAT POWER | 20 | 1 | 1 | 1,620 |  |  |  |  |  | 102 VP |
|  |  |  |  | 435 |  |  | 2 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 3 |  | 1,620 |  |  |  |  | 102 VP |
|  |  |  |  |  | 435 |  | 4 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 5 |  |  | 1,440 |  |  |  | 103 SEAT POWER |
|  |  |  |  |  |  | 1,440 | 6 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 7 | 1,260 |  |  |  |  |  | 103 SEAT POWER |
|  |  |  |  | 1.440 |  |  | 8 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 9 |  | 1,080 |  |  |  |  | 103 SEAT POWER |
|  |  |  |  |  | 1.440 |  | 10 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 11 |  |  | 1,260 |  |  |  | 102 SEAT POWER |
|  |  |  |  |  |  | 1.080 | 12 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 13 | 1,800 |  |  |  |  |  | 102 SEAT POWER |
|  |  |  |  | 900 |  |  | 14 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 15 |  | 1,260 |  |  |  |  | 102 SEAT POWER |
|  |  |  |  |  | 1.620 |  | 16 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 17 |  |  | 1,800 |  |  |  | 102 SEAT POWER |
|  |  |  |  |  |  | 1.800 | 18 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 19 | 1,620 |  |  |  |  |  | 102 SEAT POWER |
|  |  |  |  | 1.260 |  |  | 20 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 21 |  | 1,620 |  |  |  |  | 102 SEAT POWER |
|  |  |  |  |  | 1.440 |  | 22 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 23 |  |  | 1,440 |  |  |  | 102 SEAT POWER |
|  |  |  |  |  |  | 1,080 | 24 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 25 | 1,260 |  |  |  |  |  | 102 SEAT POWER |
|  |  |  |  | 900 |  |  | 26 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 27 |  | 1,080 |  |  |  |  | 102 SEAT POWER |
|  |  |  |  |  | 1,620 |  | 28 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 29 |  |  | 1,260 |  |  |  | 102 SEAT POWER |
|  |  |  |  |  |  | 1,800 | 30 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 31 | 1,800 |  |  |  |  |  | 102 SEAT POWER |
|  |  |  |  | 1,260 |  |  | 32 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 33 |  | 1,260 |  |  |  |  | 102 SEAT POWER |
|  |  |  |  |  | 1.440 |  | 34 | 1 | 20 |  |
| 101 SEAT POWER | 20 | 1 | 35 |  |  | 1,800 |  |  |  | 103 SEAT POWER |
|  |  |  |  |  |  | 1,440 | 36 | 1 | 20 |  |
| ILUX CONTROLLER | 20 | 1 | 37 | 1,000 |  |  |  |  |  | 103 SEAT POWER |
|  |  |  |  | 1.260 |  |  | 38 | 1 | 20 |  |
| CRESTRON POWER SUPPLY | 20 | 1 | 39 |  | 276 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 40 | 1 | 20 |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 42 | 1 | 20 |  |
|  | TOTAL VA |  |  | 17.815 | 6.191 | 17.640 | TOTAL KVA |  |  | 51.6 |
|  | TOTAL | AMP/PH |  | 148 | 135 | 147 | TOTAL | AMP |  | 143 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 2.3.7 - RP-1SA-3 Original Panelboard Schedule


Figure 2.3.8 - RP-1SA-3 Panelboard Worksheet
Jason Greer I Villanova University: School of Law


Figure 2.3.9 - RP-1SA-3 Revised Panelboard Schedule

| 135-Seat Classroom Feeder Sizing Worksheet |  |  |
| :--- | ---: | ---: |
| Panelboard Tag | LP-1S | RP-1SA-3 |
| Panelboard Voltage | $480 \mathrm{Y} / 277$ | $208 \mathrm{Y} / 120$ |
| Calculated Design Load (kw) | 560.5 | 62.3 |
| Calculated Design Load (kva) | 560.5 | 62.3 |
| Resultant Power Factor | 1 | 1 |
| Calculated Design Load (amps) | 674.5 | 172.9 |
| Feeder Protection Size | 700 | 175 |
| Sets | 2 | 1 |
| Wire Size |  |  |
| Phase | $3 \# 400 \mathrm{MCM}$ | $3 \# 2 / 0$ |
| Neutral | Ground | $1 \# 400 \mathrm{MCM}$ |
| Conduit Size | $\# 1 / 0$ | $\# 2 / 0$ |

Figure 2.3.10 - 135-Seat Classroom Feeder Sizing Worksheet

## Moot Courtroom

The moot courtroom is a space that will be used for mock trials, and classroom tasks such as exam taking, lectures, presentations and general discussions. The lighting design for the space is flexible and functional. One of the main goals of the new lighting design is to accent the architecture that dominates the space. There is a substantial amount of wood and points of interest on the perimeter and the ceiling.

The panels that are affected by the lighting redesign are as follows: LP-2S which is located in Electrical Room 219A on the second floor and RP-2SA-1 which is also located in 219A.

The controls for the space will be similar to those in the classroom. A scene controller equivalent to Lutron's Grafik Eye 3000 will provide scene control. There are four zones in the space, each of which will be controlled depending on the scene selected. There are also occupancy sensors in the room as a means of meeting ASHRAE 90.1 automatic shutoff criteria.

The following table outlines the overprotection, feeder and conduit information for the existing panels for the courtyard.

| Affected Moot Courtroom Panels |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Panelboard | Breaker | Feeder |  |  |  | Conduit |
|  |  | Sets | Phase | Neutral | Ground |  |
| LP-2S | 225A, 3P | 1 | 3\#4/0 | 1\#4/0 | 1\#4 | 2-1/2" |
| RP-2SA-1 | 125A, 3P | 2 | 3\#3/0 | 1\#3/0 | 1\#3 | (2) $2^{\prime \prime}$ |

Figure 2.4.1 - Moot Courtroom Affected Panelboard Information


Figure 2.4.2 - Moot Courtroom Electrical Plan
*See Appendix B for full size plan

| Moot Courtroom Scene Matrix |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: |
| Zone |  |  |  |  |  |
| Scene | A | B | C | D |  |
| General <br> Lighting | $100 \%$ | $100 \%$ | $100 \%$ | $100 \%$ |  |
| Court | $50 \%$ | $100 \%$ | $80 \%$ | $100 \%$ |  |
| Lecture | $80 \%$ | $100 \%$ | $50 \%$ | $50 \%$ |  |
| Electronic <br> Presentation | $10 \%$ | $10 \%$ | $80 \%$ | $0 \%$ |  |

Figure 2.4.3 - Moot Courtroom Scene Control Matrix
*See Appendix C for control specifications


Figure 2.4.4 - LP-2S Original Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.4.5 - LP-2S Panelboard Worksheet


Figure 2.4.6 - LP-2S Revised Panelboard Schedule


Figure 2.4.7 - RP-2SA-1 Original Panelboard Schedule

PANELBOARD SIZING WORKSHEET


Figure 2.4.8 - RP-2SA-1 Panelboard Worksheet
Jason Greer I Villanova University: School of Law

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RP-2SA-1 |  | EQUIP. GND. BUS: ISOLATED GND BUS: |  |  |  |  |  | VOLTAGE: |  | $120 / 208 \mathrm{VOLT}, 3 \mathrm{PH}, 4 \mathrm{~W}$ |
| ELEC.RM.(219A)-2ND FL. |  |  |  |  |  | 200\% |  | MAIN CIRCUIT BKR: |  | : 125 |
| SURFACE |  | NEUTRAL BUS: |  | 100\% |  |  |  | MLO: |  |  |
| FED FROM: PANEL 'LP-2S' |  | A.I.C.: | 22000 |  |  |  |  | BUS RA | ING: | 225 |
| LOAD DESCRIPTION | $\begin{array}{\|c\|} \hline \text { BKR. } \\ \text { AMPS } \end{array}$ | BKR.POLE | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 240/241 GENERAL RECEPTACLES | 20 | 1 | 1 | 1,080 |  |  |  |  |  | 238/239 GENERAL RECEPTACLES |
|  |  |  |  | 1,080 |  |  | 2 | 1 | 20 |  |
| 240/241 RECEPTACLES | 20 | 1 | 3 |  | 720 |  |  |  |  | 238/239 RECEPTACLES |
|  |  |  |  |  | 720 |  | 4 | 1 | 20 |  |
| 249/250 GENERAL RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 219C/220B GENERAL RECEPTACLES |
|  |  |  |  |  |  | 720 | 6 | 1 | 20 |  |
| 242/243 GENERAL RECEPTACLES | 20 | 1 | 7 | 1,080 |  |  |  |  |  | 220B ECW RECEPTACLE |
|  |  |  |  | 1.000 |  |  | 8 | 1 | 20 |  |
| 242/243 RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | 236/237 GENERAL RECEPTACLES |
|  |  |  |  |  | 1.080 |  | 10 | 1 | 20 |  |
| 249 WALL QUAD RECEPTACLES | 20 | 1 | 11 |  |  | 720 |  |  |  | 236/237 RECEPTACLES |
|  |  |  |  |  |  | 720 | 12 | 1 | 20 |  |
| 249 RECEPTACLE | 20 | 1 | 13 | 360 |  |  |  |  |  | 221 FLOOR QUAD RECEPTACLES |
|  |  |  |  | 720 |  |  | 14 | 1 | 20 |  |
| MOOT COURT LIGHTINGTRACK LIGHTING | 20 | 1 | 15 |  | 700 |  |  |  |  | 221 GENERAL RECEPTACLES |
|  |  |  |  |  | 720 |  | 16 | 1 | 20 |  |
| 249 RECEPTACLE | 20 | 1 | 17 |  |  | 360 |  |  |  | 234/235 GENERAL RECEPTACLES |
|  |  |  |  |  |  | 1.080 | 18 | 1 | 20 |  |
| SPARE | 20 | 1 | 19 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 20 | 1 | 20 |  |
| 221 FLOOR QUAD RECEPTACLE | 20 | 1 | 21 |  | 360 |  |  |  |  | 234/235 RECEPTACLES |
|  |  |  |  |  | 720 |  | 22 | 1 | 20 |  |
| 222 RECEPTACLES | 20 | 1 | 23 |  |  | 360 |  |  |  | 222 COPIER RECEPTACLE |
|  |  |  |  |  |  | 1,000 | 24 | 1 | 20 |  |
| 250A JUNCTION BOX | 20 | 1 | 25 | 1,000 |  |  |  |  |  | 222/250A GENERAL RECEPTACLES |
|  |  |  |  | 360 |  |  | 26 | 1 | 20 |  |
| 202 J2 | 20 | 1 | 27 |  | 1,500 |  |  |  |  | 232/233 GENERAL RECEPTACLES |
|  |  |  |  |  | 1,080 |  | 28 | 1 | 20 |  |
| 202 PS | 20 | 1 | 29 |  |  | 1,400 |  |  |  | 232/233 RECEPTACLES |
|  |  |  |  |  |  | 720 | 30 | 1 | 20 |  |
| 202 F 2 | 20 | 1 | 31 | 750 |  |  |  |  |  | 230/231 GENERAL RECEPTACLES |
|  |  |  |  | 1.080 |  |  | 32 | 1 | 20 |  |
| 202 VP | 20 | 1 | 33 |  | 435 |  |  |  |  | 230/231 RECEPTACLES |
|  |  |  |  |  | 720 |  | 34 | 1 | 20 |  |
| 202 VP | 20 | 1 | 35 |  |  | 435 |  |  |  | 228/229 GENERAL RECEPTACLES |
|  |  |  |  |  |  | 1.080 | 36 | 1 | 20 |  |
| 202 F 2 | 20 | 1 | 37 | 750 |  |  |  |  |  | PANEL 'RP-2SB' |
|  |  |  |  | 10,670 |  |  | 38 | 3 | 100 |  |
| SPARE | 20 | 1 | 39 |  |  |  |  |  |  |  |
|  |  |  |  |  | 10,420 |  | 40 |  |  |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 8,886 | 42 |  |  |  |
|  | TOTAL VA |  |  | 19,930 | 19,895 | 18,201 | TOTAL KVA |  |  | 58.0 |
|  | TOTAL | AMP/PH |  | 166 | 166 | 152 | TOTAL AMP |  |  | 161 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 2.4.9 - RP-2SA-1 Revised Panelboard Schedule

| Moot Courtroom Feeder Sizing Worksheet |  |  |
| :--- | ---: | ---: |
| Panelboard Tag | LP-2S | RP-2SA-1 |
| Panelboard Voltage | $480 \mathrm{Y} / 277$ | $208 \mathrm{Y} / 120$ |
| Calculated Design Load (kw) | 177.4 | 69.7 |
| Calculated Design Load (kva) | 177.4 | 69.7 |
| Resultant Power Factor | 1 | 1 |
| Calculated Design Load (amps) | 213.4 | 193.7 |
| Feeder Protection Size | 225 | 200 |
| Sets | 1 | 1 |
| Wire Size |  |  |
| Phase | $3 \# 4 / 0$ | $3 \# 3 / 0$ |
| Neutral | $1 \# 4 / 0$ | $1 \# 3 / 0$ |
| Ground | $\# 4$ | $\# 6$ |
| Conduit Size | $2 "$ | $2 "$ |

Figure 2.4.10 - Moot Courtroom Feeder Sizing Worksheet

## ELECTRICAL DISTRIBUTION REDESIGN

## Introduction

The current electrical distribution system for the Villanova University School of Law uses standard 42 circuit lighting and receptacle panels. Each receptacle panel is fed from a lighting panel through a transformer upstream. The existing system has nine transformers ranging in size from 30 Kva to 112.5 Kva. There are eight 480 V lighting panels and 21208 V receptacle panels. These components are part of the regular power system.

The emergency power system was not redesigned because it would not reduce the number of transformers. It would have only used more panels. The other branch that was not redesigned was the receptacle panels for the basement kitchen. A small transformer is dedicated to the kitchen so switching to a distribution panel would only require an additional piece of equipment and result in no reduction of transformers.

The idea behind the redesign is that by changing from standard lighting panels to distribution panels the number of transformers will be reduced from eight to three resulting in a reduction of cost. Also, the transformers can be installed in the room with the distribution panel which will significantly cut down the length of run for the large feeder that runs from the transformer to the first panel. The longest run can now be the primary side of the transformer which will be a smaller conductor because of the higher voltage.

The following pages will show the original and redesigned single line diagram, calculations, original and new schedules as well as a cost analysis. Finally, an analysis section will discuss the benefits of each section and present all conclusions. For figures that are illegible, see Appendix D for full size figures.

In the following schedules, the components in gray are the ones that were affected by the system redesign.

## Original System Schedules

| ORIGINAL TRANSFORMER SCHEDULE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TAG | PRIMARY VOLTAGE | SECONDARY VOLTAGE | SIZE | TYPE | TEMP. RISE | TAPS | MOUNTING | REMARKS |
| XD-1 | $13.2 \mathrm{kV}, 3 \mathrm{P}, 3 \mathrm{~W}$ | 480Y/277V, 3P, 4W | 1500kVA | Silicone-based dielectric filled | $55^{\circ} \mathrm{C}$ | (4) $2.5 \%$ Taps <br> (2) Up \& (2) Dn | Concrete Pad Mount (outside) |  |
| XS-1 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-2 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-3 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-4 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-5 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) 2.5\% Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-6 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 30kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-7 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-8 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-9 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-10 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-11 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5 kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |

Figure 3.1.1 - Original Distribution System Transformer Schedule

| TAG | FROM | TO | $\begin{gathered} \text { NO. OF } \\ \text { SETS } \end{gathered}$ | ORIGINAL FEEDER SCHEDULE |  |  |  |  |  |  |  |  |  |  | SIZE OF OVERCURRENT PROTECTION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { CONDUIT } \\ & \text { (PER SET) } \end{aligned}$ |  | CONDUCTORS (PER SET) |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | PHASE CONDUCTORS |  |  | NEUTRAL CONDUCTORS |  |  | GROUND CONDUCTORS |  |  |  |
|  |  |  |  | SIZE | TYPE | No. | SIZE | TYPE | No. | SIZE | TYPE | No. | SIZE | TYPE |  |
| 1 | UTILITY | XD-1 | 1 | $4{ }^{\text {" }}$ | PVC | 3 | 4/0 | -- | -- | -- | -- | 1 | 2 | -- | -- |
| 2 | UTILITY | XD-1 | 1 | $4{ }^{\prime \prime}$ | PVC | 3 | 4/0 | -- | -- | -- | -- | 1 | 2 | -- | -- |
| 3 | XD-1 | MDB | 7 | $4{ }^{\prime \prime}$ | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 350 | CU THWN | -- |
| 4 | XD-1 | Disc. Sw | 1 | 1.5" | EMT | 3 | 1/0 | CU THWN | 1 | 3 | CU THWN | 1 | 6 | CU THWN | -- |
| 5 | Disc. Sw | Fire Pump | 1 | 1.5" | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 800A Fuse |
| 6 | MDB | LP-1N | 2 | 2" | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 3 | CU THWN | 400A, 3P |
| 7 | LP-1N | XS-1 | 1 | 1.5" | EMT | 3 | 1/0 | CU THWN | 0 | -- | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 8 | XS-1 | RP-1NA | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 250A, 3P |
| 9 | RP-1NA | RP-1NB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 10 | LP-1N | LP-2N | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 11 | LP-2N | XS-2 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 70A, 3P |
| 12 | XS-2 | RP-2NA | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 13 | RP-2NA | RP-2NB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 14 | LP-1N | LP-3N | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 15 | LP-3N | XS-3 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 70A, 3P |
| 16 | XS-3 | RP-3NA | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 17 | RP-3NA | RP-3NB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 50A, 3P |
| 18 | MDB | LP-1S | 1 | 3 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 19 | LP-1S | XS-4 | 1 | 1.5 | EMT | 3 | 1/0 | CU THWN | 0 | -- | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 20 | XS-4 | RP-1SA-1 | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 125A, 3P |
| 21 | RP-1SA-1 | RP-1SA-2 | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 125A, 3P |
| 22 | RP-1SA-2 | RP-1SA-3 | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 125A, 3P |
| 23 | RP-1SA-1 | RP-1SB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 24 | MDB | XS-5 | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 225A, 3P |
| 25 | XS-5 | $\begin{gathered} \text { RP-K } \\ (\text { Sec.1) } \end{gathered}$ | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 150A, 3P |
| 26 | $\begin{gathered} \text { RP-K } \\ (\mathrm{Sec} .1) \\ \hline \end{gathered}$ | $\begin{gathered} \text { RP-K } \\ (\mathrm{Sec} .2) \end{gathered}$ | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 150A, 3P |
| 27 | MDB | LP-BN | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 28 | LP-BN | XS-6 | 1 | 0.75 | EMT | 3 | 6 | CU THWN | 0 | -- | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 29 | XS-6 | RP-BN | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 30 | MDB | LP-BS | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 31 | LP-BS | XS-7 | 1 | 1.5 | EMT | 3 | 1/0 | CU THWN | 0 | -- | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 32 | XS-7 | RP-BS | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 34 | RP-BS | RP-BSA | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 35 | MDB | ELEV. | 1 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 6 | CU THWN | 800A Fuse |
| 36 | MDB | Elev-BN | 1 | 3 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 37 | MDB | LP-2S | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 38 | LP-2S | XS-8 | 1 | 1.5 | EMT | 3 | 1/0 | CU THWN | 0 | -- | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 39 | XS-8 | RP-2SA-1 | 2 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 3 | CU THWN | 125A, 3P |
| 40 | RP-2SA-1 | RP-2SA-2 | 2 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 3 | CU THWN | 125A, 3P |
| 41 | RP-2SA-2 | RP-2SA-3 | 2 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 3 | CU THWN | 125A, 3P |
| 42 | RP-2SA-1 | RP-2SB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 43 | MDB | LP-3S | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 44 | LP-3S | XS-9 | 1 | 1.5 | EMT | 3 | 1/0 | CU THWN | 0 | -- | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 45 | XS-9 | RP-3SA-1 | 1 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 46 | RP-3SA-1 | RP-3SA-2 | 1 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 47 | RP-3SA-2 | RP-3SA-3 | 1 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 48 | RP-3SA-1 | RP-3SB | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 49 | MDB | Snow Mlt. | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 50 | MDB | ATS-LS | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 51 | ATS-LS | GEN | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 52 | ATS-LS | EDP-BS | 1 | $2 . .5$ | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 53 | EDP-BS | XS-10 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 54 | XS-10 | ERP-BS | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 100A, 3P |
| 55 | ERP-BS | ERP-1S | 1 | 2 | EMT | 3 | 1/0 | CUTHWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 60A, 3P |
| 56 | ERP-1S | ERP-3S | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 50A, 3P |
| 57 | EDP-BS | ELP-1S | 1 | 1.5 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 50A, 3P |
| 58 | ELP-3S | ELP-3S | 1 | 1 | EMT | 3 | 6 | CUTHWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 59 | EDP-BS | ELP-1N | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 60 | ELP-1N | ELP-3N | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 61 | EDP-BS | ELP-BS | 1 | 1 | EMT | 3 | 6 | CUTHWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 62 | MDB | MCC | 2 | 3 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 1 | CU THWN | 750A, 3P |
| 63 | MDB | DP-PH | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 64 | MDB | ATS-NLS | 1 | 1.25 | EMT | 3 | 4 | CUTHWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 65 | ATS-NLS | GEN | 1 | 1.25 | EMT | 3 | 4 | CUTHWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 70A, 3P |
| 66 | ATS-NLS | ENDPH-BS | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 67 | ENDPH-BS | XS-11 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 125A, 3P |
| 68 | XS-11 | ENDPL-BS | 1 | 2 | EMT | 3 | 1/0 | CUTHWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 250A, 3P |
| 69 | ENDPL-BS | ENP-MDF | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 70 | ENDPL-BS | ENP-MDF2 | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 71 | ENDPL-BS | ENP-BS | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 72 | ENDPL-BS | ENP-1S | 1 | 1.25 | EMT | 3 | 4 | CUTHWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 73 | ENP-1S | ENP-3S | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |

Figure 3.1.2 - Original Distribution System Feeder Schedule

## Original System Panel Board Schedules

Below are the original panel board schedules for all panels that are used as a distributions panel. These are the panels that were affected by the redesign because of the elimination of the load from the downstream panel.

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: LP-1N | EQUIP. GND. BUS: $\square$ |  |  |  |  | VOLTAGE: |  |  |  | 480/277 VOLT, 3PH, 4W |
| LOCATION: ELEC.RM.(188)-1ST FL. | ISOLATED GND BUS: |  |  |  |  | 200\% | $\square$ | MAIN CIRCUIT BKR: |  |  |
| MOUNTING: SURFACE |  | NEUTRAL BUS: |  | 100\% |  |  |  | MLO: <br> BUS RATING: |  | 400 |
| FED FROM: SWBD 'MDB' |  | A.I.C.: | 42000 |  |  |  |  |  |  |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | CKT. NO. | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | BKR. POLE | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-1-3 |  |  | 1 | 3,713 |  |  |  |  |  | RF-1-3 |
|  |  |  |  | 1.275 |  |  | 2 |  |  |  |
|  | 30 | 3 | 3 |  | 3,713 |  |  |  |  |  |
|  |  |  |  |  | 1,275 |  | 4 | 3 | 15 |  |
|  |  |  | 5 |  |  | 3,713 |  |  |  |  |
|  |  |  |  |  |  | 1.275 | 6 |  |  |  |
| $\begin{gathered} \text { LIGHTING } \\ \text { OFFICE SPACE } \\ \hline \end{gathered}$ | 20 | 1 | 7 | 4,000 |  |  |  |  |  | LIGHTINGOFFICE CORRIDOR |
|  |  |  |  | 3.176 |  |  | 8 | 1 | 20 |  |
| $\begin{gathered} \text { LIGHTING } \\ \text { MAIN CORRIDOR } \end{gathered}$ | 20 | 1 | 9 |  | 2,500 |  |  |  |  | LIGHTINGOFFICE SPACE |
|  |  |  |  |  | 1.400 |  | 10 | 1 | 20 |  |
| LIGHTINGMAIN SEATING AREA | 20 | 1 | 11 |  |  | 1,400 |  |  |  | LIGHTING CHAPEL |
|  |  |  |  |  |  | 1,800 | 12 | 1 | 20 |  |
|  | 20 | 1 | 13 |  |  |  |  |  |  | LIGHTINGEXTERIOR READING ROOM |
|  |  |  |  | 1.250 |  |  | 14 | 1 | 20 |  |
| SPARE | 20 | 1 | 15 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 16 | 1 | 20 |  |
| SPARE | 20 | 1 | 17 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 18 | 1 | 20 |  |
| SPARE | 20 | 1 | 19 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 20 | 1 | 20 |  |
| SPARE | 20 | 1 | 21 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 22 | 1 | 20 |  |
| SPARE | 20 | 1 | 23 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 24 | 1 | 20 |  |
| SPARE | 20 | 1 | 25 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| SPARE | 20 | 1 | 27 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| SPARE | 20 | 1 | 29 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | PANEL 'LP-3N' |
|  |  |  |  | 40,313 |  |  | 32 | 3 | 150 |  |
| SPARE | 20 | 1 | 33 |  |  |  |  |  |  |  |
|  |  |  |  |  | 37,544 |  | 34 |  |  |  |
| LIGHTING CONTROL PANELLCP-1B | 20 | 1 | 35 |  |  | 1,000 |  |  |  |  |
|  |  |  |  |  |  | 36,920 | 36 |  |  |  |
| PANEL 'RP-1NA' ( 75 KVA XFMR) | 125 | 3 | 37 | 23,511 |  |  |  |  |  | PANEL 'LP-2N' |
|  |  |  |  | 26,681 |  |  | 38 | 3 | 150 |  |
|  |  |  | 39 |  | 18,645 |  |  |  |  |  |
|  |  |  |  |  | 28,445 |  | 40 |  |  |  |
|  |  |  | 41 |  |  | 18,837 |  |  |  |  |
|  |  |  |  |  |  | 25,239 | 42 |  |  |  |
|  | TOTAL VA |  |  | 103,919 | 93,522 | 90,184 | TOTAL KVA |  |  | 287.6 |
|  | TOTAL | AMP/PH |  | 375 | 338 | 326 | TOTAL | AMP |  | 346 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.1 - LP-1N Original Panelboard Schedule


Figure 3.2.2 - RP-1NA Original Panelboard Schedule


Figure 3.2.3 - LP-2N Original Panelboard Schedule


Figure 3.2.4 - RP-2NA Original Panelboard Schedule


Figure 3.2.5 - LP-3N Original Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RP-3NA <br> ELEC.RM.(366)-3RD FL <br> SURFACE <br> PANEL 'LP-3N' |  | EQUIP. GND. BUS: $\square$  <br> ISOLATED GND BUS: $\square$  <br> NEUTRAL BUS: $\mathbf{1 0 0 \%}$ $\square$ <br> A.I.C.: 22,000   |  |  |  | 200\% |  | VOLTAGE: <br> MAIN CIRCUIT BKR: |  | $120 / 208$ VOLT, 3PH, 4W |
|  |  |  |  |  |  |  | 150A |  |  |
|  |  |  |  |  |  |  | MLO: |  |  |
|  |  |  |  |  |  |  | BUS RA | ING: | 225A |
|  | BKR. | BKR. POLE | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \\ & \hline \end{aligned}$ | $\begin{array}{\|c} \hline \text { BKR. } \\ \text { AMPS } \\ \hline \end{array}$ | LOAD DESCRIPTION |
| LOAD DESCRIPTION | AMPS |  |  | A | B |  |  |  |  |  | C |
| 365 RECEPTACLES | 20 | 1 | 1 | 360 |  |  |  |  |  |  | ROOF RECEPTACLES |
|  |  |  |  | 360 |  |  |  | 2 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 3 |  | 360 |  |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  | 1,440 |  | 4 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 367 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 6 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 7 | 720 |  |  |  |  |  | 360 B RECEPTACLES |
|  |  |  |  | 1.260 |  |  | 8 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | 360 RECEPTACLES |
|  |  |  |  |  | 1,440 |  | 10 | 1 | 20 |  |
| 370/371 RECEPTACLES | 20 | 1 | 11 |  |  | 1,260 |  |  |  | 372 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 12 | 1 | 20 |  |
| 370 RECEPTACLES | 20 | 1 | 13 | 1,080 |  |  |  |  |  | 368 RECEPTACLES\& DOOR HOLDERS |
|  |  |  |  | 1.460 |  |  | 14 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 15 |  | 720 |  |  |  |  | FP-3-4 |
|  |  |  |  |  | 800 |  | 16 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 17 |  |  | 720 |  |  |  | TE-3-1 |
|  |  |  |  |  |  | 299 | 18 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 19 | 720 |  |  |  |  |  | TF-3-1 |
|  |  |  |  | 500 |  |  | 20 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 21 |  | 720 |  |  |  |  | FP-3-3 |
|  |  |  |  |  | 830 |  | 22 | 1 | 15 |  |
| 374 RECEPTACLES | 20 | 1 | 23 |  |  | 720 |  |  |  | UH-1 |
|  |  |  |  |  |  | 506 | 24 | 1 | 15 |  |
| 376 COPIER | 20 | 1 | 25 | 1,000 |  |  |  |  |  | J-BOX, VAV |
|  |  |  |  | 1,000 |  |  | 26 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 27 |  | 900 |  |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  | 720 |  | 28 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 29 |  |  | 720 |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  |  | 720 | 30 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 31 | 720 |  |  |  |  |  | LIGHTING 365 PENDANTS |
|  |  |  |  | 322 |  |  | 32 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 33 |  | 900 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 34 | 1 | 20 |  |
| 375 RECEPTACLES | 20 | 1 | 35 |  |  | 540 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 36 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 37 | 720 |  |  |  |  |  | PANEL 'RP-3NB' |
|  |  |  |  | 11.225 |  |  | 38 | 3 | 50 |  |
| 365 RECEPTACLES | 20 | 1 | 39 |  | 720 |  |  |  |  |  |
|  |  |  |  |  | 11.056 |  | 40 |  |  |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 9,413 | 42 |  |  |  |
|  | TOTAL VA |  |  | 21,447 | 21,326 | 18,498 | TOTAL KVA |  |  | 61.271 |
|  | TOTAL | AMP/PH |  | 179 | 178 | 154 | TOTAL | AMP |  | 170 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.6 - RP-3NA Original Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LP-1S | EQUIP. GND. BUS: |  |  |  |  | VOLTAGE: |  |  |  | 480/277 VOLT, 3PH, 4W |
| ELEC.RM.(119A)-1ST FL. |  | ISOLATED GND BUS: |  |  |  | 200\% | MAIN CIRCUIT BKR: |  |  |  |
| MOUNTING: SURFACE |  | NEUTR | BUS: | 100\% |  |  | $\square$ | MLO: |  |  |
| FED FROM: SWBD 'MDB' |  | A.I.C.: | 42000 |  |  |  |  | BUS RA | NG: | 600 |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | CKT. NO. | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-1-1 |  |  | 1 | 3,713 |  |  |  |  |  | RF-1-1 |
|  |  |  |  | 2.015 |  |  | 2 |  |  |  |
|  | 30 | 3 | 3 |  | 3,713 |  |  |  |  |  |
|  |  |  |  |  | 2.015 |  | 4 | 1 | 15 |  |
|  |  |  | 5 |  |  | 3,713 |  |  |  |  |
|  |  |  |  |  |  | 2.015 | 6 |  |  |  |
| $\begin{aligned} & \text { LIGHTING } \\ & \text { CORE AREA } \end{aligned}$ | 20 | 1 | 7 | 3,056 |  |  |  |  |  | LIGHTING135 CLASSROOM |
|  |  |  |  | 2,576 |  |  | 8 | 1 | 20 |  |
| LIGHTING OFFICES | 20 | 1 | 9 |  | 3,040 |  |  |  |  | LIGHTING90 CLASSROOM |
|  |  |  |  |  | 1,902 |  | 10 | 1 | 20 |  |
| LIGHTING OFFICES | 20 | 1 | 11 |  |  | 1,840 |  |  |  | LIGHTING55 CLASSROOM |
|  |  |  |  |  |  | 2,008 | 12 | 1 | 20 |  |
| LIGHTINGOFFICE CORRIDORS | 20 | 1 | 13 | 1,800 |  |  |  |  |  | LIGHTING MAIN STAIRS |
|  |  |  |  | 2,500 |  |  | 14 | 1 | 20 |  |
| LIGHTINGMAIN CORRIDOR AND LOBBY | 20 | 1 | 15 |  | 2,800 |  |  |  |  | LIGHTINGSOUTH STAIRS |
|  |  |  |  |  | 2,500 |  | 16 | 1 | 20 |  |
| LIGHTINGOFFICE SPACE | 20 | 1 | 17 |  |  | 3,200 |  |  |  | LIGHTINGNORTH STAIRS |
|  |  |  |  |  |  | 1,250 | 18 | 1 | 20 |  |
| LIGHTING ATRIUM | 20 | 1 | 19 | 350 |  |  |  |  |  | ENTRY LIGHTING |
|  |  |  |  | 800 |  |  | 20 | 1 | 20 |  |
| VERTICAL COVE LIGHTS BASEMENT THRU 3RD FLOOR | 20 | 1 | 21 |  | 1,000 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 22 | 1 | 20 |  |
| $\begin{aligned} & \text { 151A,B J-BOXES } \\ & \text { HAND DRYERS } \end{aligned}$ | 20 | 1 | 23 |  |  | 3,048 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 24 | 1 | 20 |  |
| 118B J-BOXES HAND DRYERS | 20 | 1 | 25 | 3,048 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| 118A J-BOXES HAND DRYERS | 20 | 1 | 27 |  | 3,048 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| SPARE | 20 | 1 | 29 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 32 | 3 | 100 |  |
| SPARE | 20 | 1 | 33 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 34 |  |  |  |
| LIGHTING CONTROL PANELLCP-1A | 20 | 1 | 35 |  |  | 1,000 |  |  |  |  |
|  |  |  |  |  |  |  | 36 |  |  |  |
| PANELS 'RP-1SA-1' \& 'RP-1SA-2' ( 75 KVA XFMR) | 125 | 3 | 37 | 38,782 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 38 | 3 | 50 |  |
|  |  |  | 39 |  | 40,015 |  |  |  |  |  |
|  |  |  |  |  |  |  | 40 |  |  |  |
|  |  |  | 41 |  |  | 36,606 |  |  |  |  |
|  |  |  |  |  |  |  | 42 |  |  |  |
|  | TOTAL VA |  |  | 8.640 | 0,033 | 5,680 | TOTAL KVA |  |  | 173.4 |
|  | TOTAL | AMP/PH |  | 212 | 217 | 197 | TOTAL | AMP |  | 209 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.7 - LP-1S Original Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: $\quad$ RP-1SA-1 | EQUIP. GND. BUS: |  |  |  |  |  | VOLTAGE: |  |  | $120 / 208$ VOLT, 3PH, 4W |
| LOCATION: ELEC.RM.(119A)-1ST FL. | ISOLATED GND BUS: |  |  |  |  | 200\% | MAIN CIRCUIT BKR: |  |  | : 125 |
| MOUNTING: SURFACE | NEUTRAL BUS: |  |  | 100\% |  |  |  | MLO: $\quad \square$ |  |  |
| FED FROM: PANEL 'LP-1S' |  | A.I.C.: | 22500 |  |  |  |  | BUS RA | ING: | 225 |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 143/144/146 GENERAL RECEPTS. | 20 | 1 | 1 | 1,260 |  |  |  |  |  | 122/123 GENERAL RECEPTACLES |
|  |  |  |  | 1.080 |  |  | 2 | 1 | 20 |  |
| 148/149A GENERAL RECEPTACLES | 20 | 1 | 3 |  | 1,260 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 4 | 1 | 20 |  |
| 141/142 COMPUTER RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 120B EWC RECEPTACLE |
|  |  |  |  |  |  | 500 | 6 | 1 | 20 |  |
| 141/142 GENERAL RECEPTACLES | 20 | 1 | 7 | 1,260 |  |  |  |  |  | 121/137 COMPUTER RECEPTACLES |
|  |  |  |  | 1.080 |  |  | 8 | 1 | 20 |  |
| 148/149A,B COMPUTER RECEPTACLES | 20 | 1 | 9 |  | 1,080 |  |  |  |  | 121 COMPUTER RECEPTACLES |
|  |  |  |  |  | 1.080 |  | 10 | 1 | 20 |  |
| 147/149,B GENERAL RECEPTACLES | 20 | 1 | 11 |  |  | 900 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 12 | 1 | 20 |  |
| 140/139 GENERAL RECEPTACLES | 20 | 1 | 13 | 1,080 |  |  |  |  |  | 121 FAX RECEPTACLE |
|  |  |  |  | 500 |  |  | 14 | 1 | 20 |  |
| 139/140 COMPUTER RECEPTACLES | 20 | 1 | 15 |  | 720 |  |  |  |  | 121 COPY RECEPTACLE |
|  |  |  |  |  | 1,000 |  | 16 | 1 | 20 |  |
| 150 COMPUTER RECEPTACLES | 20 | 1 | 17 |  |  | 720 |  |  |  | CUH-1-3 |
|  |  |  |  |  |  | 345 | 18 | 1 | 15 |  |
| 138/150 GENERAL RECEPTACLES | 20 | 1 | 19 | 1,080 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 20 | 1 | 20 |  |
| 138/150 COMPUTER RECEPTACLES | 20 | 1 | 21 |  | 720 |  |  |  |  | 122/123 COMPUTER RECEPTACLES |
|  |  |  |  |  | 720 |  | 22 | 1 | 20 |  |
| CONVENIANCE RECEPTACLECOFFEE BAR | 20 | 1 | 23 |  |  | 360 |  |  |  | 124/125 GENERAL RECEPTACLES |
|  |  |  |  |  |  | 1.080 | 24 | 1 | 20 |  |
| 119C/121,A/137 GENERAL RECEPTACLES | 20 | 1 | 25 | 1,260 |  |  |  |  |  | 124/125 COMPUTER RECEPTACLES |
|  |  |  |  | 720 |  |  | 26 | 1 | 20 |  |
| 138A JUNCTION BOX | 20 | 1 | 27 |  | 1,000 |  |  |  |  | 126/127/128/129 GEN. RECEPTS |
|  |  |  |  |  | 1,260 |  | 28 | 1 | 20 |  |
| 121A JUNCTION BOX | 20 | 1 | 29 |  |  | 1,000 |  |  |  | 126/127 COMPUTER RECEPTACLES |
|  |  |  |  |  |  | 720 | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | 127/128 COMPUTER RECEPTACLES |
|  |  |  |  | 720 |  |  | 32 | 1 | 20 |  |
| 149 AV | 20 | 1 | 33 |  | 1,500 |  |  |  |  | 121B/129 COMPUTER RECEPTACLES |
|  |  |  |  |  | 540 |  | 34 | 1 | 20 |  |
| 149 AV | 20 | 1 | 35 |  |  | 1,500 |  |  |  | 130 COMPUTER RECEPTACLES |
|  |  |  |  |  |  | 540 | 36 | 1 | 20 |  |
| WIREMOLD 6000 | 20 | 1 | 37 | 1,260 |  |  |  |  |  | PANEL 'RP-1SB' |
|  |  |  |  | 13.522 |  |  | 38 | 3 | 100 |  |
| WIREMOLD 6000 | 20 | 1 | 39 |  | 1,260 |  |  |  |  |  |
|  |  |  |  |  | 13,380 |  | 40 |  |  |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 14.446 | 42 |  |  |  |
|  | TOTAL VA |  |  | 24,822 | 25,520 | 22,831 | TOTAL KVA |  |  | 73.2 |
|  | TOTAL AMP/PHASE |  |  | 207 | 213 | 190 | TOTAL | AMP |  | 203 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.8 - LP-1S Original Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: LP-BN | EQUIP. GND. BUS: |  |  |  |  | VOLTAGE: |  |  |  | 480/277 VOLT, 3PH, 4W |
| LOCATION: ELEC.RM.(L29)-BSMT | ISOLATED GND BUS: |  |  |  |  | 200\% | $\square$ | MAIN CIRCUIT BKR: |  | 225 |
| MOUNTING: SURFACE |  | NEUTRAL BUS: |  | 100\% |  |  |  | MLO: |  |  |
| FED FROM: SWBD 'MDB' |  | A.l.C.: | 42000 |  |  |  |  | BUS RA | G: |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-L-1 |  |  | 1 | 3,713 |  |  |  |  |  | RF-L-1 |
|  |  |  |  | 2.920 |  |  | 2 |  |  |  |
|  | 30 | 3 | 3 |  | 3,713 |  |  |  |  |  |
|  |  |  |  |  | 2.920 |  | 4 | 3 | 30 |  |
|  |  |  | 5 |  |  | 3,713 |  |  |  |  |
|  |  |  |  |  |  | 2.920 | 6 |  |  |  |
| SPARE | 20 | 1 | 7 | 900 |  |  |  |  |  | SPARE |
|  |  |  |  | 265 |  |  | 8 | 1 | 20 |  |
| SPARE | 15 | 3 | 9 |  | 900 |  |  |  |  | SPARE |
|  |  |  |  |  | 265 |  | 10 | 1 | 20 |  |
| SPARE | 20 | 1 | 11 |  |  | 922 |  |  |  | SPARE |
|  |  |  |  |  |  | 265 | 12 | 1 | 20 |  |
| SP-1 | 15 | 1 | 13 | 795 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 14 | 1 | 20 |  |
| SP-2 | 15 | 1 | 15 |  | 795 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 16 | 1 | 20 |  |
| LIGHTINGSTE CHECKING AND MECH ROOM | 20 | 1 | 17 |  |  | 920 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 18 | 1 | 20 |  |
| LIGHTINGBASEMENT STACKS | 20 | 1 | 19 | 2,680 |  |  |  |  |  | LIGHTING <br> MAIL ROOM WORKSPACES |
|  |  |  |  | 3.512 |  |  | 20 | 1 | 20 |  |
| LIGHTING <br> BASEMENT STACKS | 20 | 1 | 21 |  | 2,744 |  |  |  |  | LIGHTING <br> MAIN LOBBY AREA |
|  |  |  |  |  | 2.000 |  | 22 | 1 | 20 |  |
| LIGHTINGCLASSROOM SPACES | 20 | 1 | 23 |  |  | 2,000 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 24 | 1 | 20 |  |
| LIGHTINGCIRCULATION SPACE | 20 | 1 | 25 | 2,016 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| LIGHTING MOVING STACKS | 20 | 1 | 27 |  | 2,880 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| LIGHTINGMAIN MECHANICAL ROOM | 20 | 1 | 29 |  |  | 1,400 |  |  |  | LIGHTINGMECH ROOM AND RESTROOM |
|  |  |  |  |  |  | 1.000 | 30 | 1 | 20 |  |
| LIGHTINGBASEMENT STACKS | 20 | 1 | 31 | 2,824 |  |  |  |  |  | EXTRA |
|  |  |  |  | 2,500 |  |  | 32 | 1 | 20 |  |
| LIGHTING CONTROL PANELLCP-0A | 20 | 1 | 33 |  | 1,000 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 34 | 1 | 20 |  |
| L24A,BHAND DRYERS | 20 | 1 | 35 |  |  | 3,048 |  |  |  | COMPACTOR |
|  |  |  |  |  |  | 1.275 | 36 | 3 | 15 |  |
| PANEL 'RP-BN' (30 KVA XFMR) | 50 | 3 | 37 | 11,218 |  |  |  |  |  |  |
|  |  |  |  | 1.275 |  |  | 38 |  |  |  |
|  |  |  | 39 |  | 13,077 |  |  |  |  |  |
|  |  |  |  |  | 1,275 |  | 40 |  |  |  |
|  |  |  | 41 |  |  | 10,838 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 42 | 1 | 20 |  |
|  | TOTAL VA |  |  | 4,618 | 31.569 | 28,301 | TOTAL KVA |  |  | 94.5 |
|  | TOTAL AMP/PHASE |  |  | 125 | 114 | 102 | TOTAL | AMP |  | 114 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.9 - LP-BN Original Panelboard Schedule


Figure 3.2.10 - LP-BS Original Panelboard Schedule


Figure 3.2.11 - RP-BS Original Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LP-2S | EQUIP. GND. BUS: |  |  |  |  | VOLTAGE: |  |  |  | 480/277 VOLT, 3PH, 4W |
| : ELEC.RM.(219A)-2ND FL. |  | ISOLATED GND BUS: |  |  |  | 200\% | $\square$ | MAIN CIRCUIT BKR: |  | 225 |
| SURFACE |  | NEUTRAL BUS: |  | 100\% |  |  |  | MLO: |  |  |
| FED FROM: PANEL 'LP-1S' |  | A.I.C.: | 42000 |  |  |  |  | BUS RA | G: |  |
| LOAD DESCRIPTION | $\begin{gathered} \text { BKR. } \\ \text { AMPS } \end{gathered}$ | BKR. <br> POLE | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | CKT. NO. | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| SF-2-1 |  |  | 1 | 3,713 |  |  |  |  |  | RF-2-1 |
|  |  |  |  | 1.275 |  |  | 2 |  |  |  |
|  | 30 | 3 | 3 |  | 3,713 |  |  |  |  |  |
|  |  |  |  |  | 1,275 |  | 4 | 3 | 15 |  |
|  |  |  | 5 |  |  | 3,713 |  |  |  |  |
|  |  |  |  |  |  | 1,275 | 6 |  |  |  |
| $\begin{aligned} & \text { LIGHTING } \\ & \text { CORE AREA } \end{aligned}$ | 20 | 1 | 7 | 3,840 |  |  |  |  |  | LIGHTING90 CLASSROOM |
|  |  |  |  | 1,902 |  |  | 8 | 1 | 20 |  |
| LIGHTING OFFICES | 20 | 1 | 9 |  | 3,800 |  |  |  |  | LIGHTING50 CLASSROOM |
|  |  |  |  |  | 2,008 |  | 10 | 1 | 20 |  |
| LIGHTINGMAIN LOBBY AND MAIN CORRIDOR | 20 | 1 | 11 |  |  | 2,750 |  |  |  | LIGHTINGOFFICE AREAS |
|  |  |  |  |  |  | 3,696 | 12 | 1 | 20 |  |
| LIGHTING MOOT COURT | 20 | 1 | 13 | 1,200 |  |  |  |  |  | LIGHTING ATRIUM |
|  |  |  |  | 336 |  |  | 14 | 1 | 20 |  |
| $\begin{gathered} \text { LIGHTING } \\ \text { MOOT COURT } \end{gathered}$ | 20 | 1 | 15 |  | 600 |  |  |  |  | LIGHTING ATRIUM |
|  |  |  |  |  | 900 |  | 16 | 1 | 20 |  |
| LIGHTINGMOOT COURT | 20 | 1 | 17 |  |  | 160 |  |  |  | LIGHTING ATRIUM |
|  |  |  |  |  |  | 900 | 18 | 1 | 20 |  |
| $\begin{gathered} \text { LIGHTING } \\ \text { MOOT COURT } \end{gathered}$ | 20 | 1 | 19 | 300 |  |  |  |  |  | LIGHTING220A CORRIDOR |
|  |  |  |  | 924 |  |  | 20 | 1 | 20 |  |
| LIGHTINGOFFICE CORRIDOR | 20 | 1 | 21 |  | 1,450 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 22 | 1 | 20 |  |
| $\begin{gathered} 218 \mathrm{~A} \\ \text { HAND DRYERS } \end{gathered}$ | 20 | 1 | 23 |  |  | 3,048 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 24 | 1 | 20 |  |
| $\begin{gathered} 218 \mathrm{~B} \\ \text { HAND DRYERS } \end{gathered}$ | 20 | 1 | 25 | 3,048 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| 248A,BHAND DRYERS | 20 | 1 | 27 |  | 3,048 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| 251A,BHAND DRYERS | 20 | 1 | 29 |  |  | 3,048 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 32 | 1 | 20 |  |
| SPARE | 20 | 1 | 33 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 34 | 1 | 20 |  |
| $\begin{aligned} & \hline \text { LIGHTING CONTROL PANEL } \\ & \text { LCP-1A } \end{aligned}$ | 20 | 1 | 35 |  |  | 1,000 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 36 | 1 | 20 |  |
| PANELS 'RP-2SA-1' \& 'RP-2SA-2' <br> ( 75 KVA XFMR) | 125 | 3 | 37 | 34,270 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 38 | 1 | 20 |  |
|  |  |  | 39 |  | 32,620 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 40 | 1 | 20 |  |
|  |  |  | 41 |  |  | 30,596 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 42 | 1 | 20 |  |
|  | TOTAL VA |  |  | 0,808 | 49,414 | 50,186 | TOTAL KVA |  |  | 150.4 |
|  | TOTAL | AMP/PH |  | 183 | 178 | 181 | TOTAL | AMP |  | 181 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.2.12 - LP-2S Original Panelboard Schedule


Figure 3.2.13 - RP-2SA-1 Original Panelboard Schedule


Figure 3.2.14 - LP-3S Original Panelboard Schedule


Figure 3.2.15 - RP-3SA-1 Original Panelboard Schedule

Original Distribution System Single Line Diagram


Figure 3.3.1 - Original Distribution System Single Line
*See Appendix D for full size single line

## Redesign Calculations

| DL-1 |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- | :--- | :--- |
| Redesign Equipment Sizing |  |  |  |  |  |  |  |  |
| PANEL | kVA | Amps | Amps |  |  |  |  |  |
| (growth) | Brk. | Bus | Feeder (THWN) | Grnd. | Conduit |  |  |  |
| LP-BN | 59.4 | 71 | 82.1 | 90 | 100 | (4) \#3 | $\# 8$ | $1-1 / 4^{\prime \prime}$ EMT |
| LP-1N | 31.5 | 38 | 43.6 | 50 | 100 | (4) \#8 | $\# 10$ | $3 / 4^{\prime \prime}$ EMT |
| LP-2N | 36.6 | 44 | 50.6 | 60 | 100 | (4) \#6 | $\# 10$ | $3 / 4^{\prime \prime}$ EMT |
| LP-3N | 53.5 | 64 | 74.0 | 80 | 100 | (4) \#4 | $\# 8$ | $11^{\prime}$ EMT |
| Total | $\mathbf{1 8 1}$ | $\mathbf{2 1 8}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | (4) 300 MCM | $\# 4$ | 2-1/2" EMT |

Figure 3.4.1 - Design Calculation for DL-1

| DL-2Redesign Equipment Sizing |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL | kVA | Amps | Amps (growth) | Brk. | Bus | Feeder (THWN) | Grnd. | Conduit |
| LP-BS | 97.5 | 117 | 134.9 | 150 | 225 | (4) $1 / 0$ | \#6 | 1-1/2" EMT |
| LP-1S | 58.0 | 70 | 80.2 | 90 | 100 | (4) \#3 | \#8 | 1-1/4" EMT |
| LP-2S | 52.9 | 64 | 73.2 | 80 | 100 | (4) \#4 | \#8 | 1" EMT |
| LP-3S | 51.2 | 62 | 70.8 | 80 | 100 | (4) \#4 | \#8 | 1" EMT |
| Total | 260 | 312 | 359 | 400 | 400 | (4) 500 MCM | \#3 | 3" EMT |

Figure 3.4.2 - Design Calculation for DL-2

| DR-1 <br> Redesign Equipment Sizing |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL | kVA | Amps | Amps (growth) | Brk. | Bus | Feeder (THWN) | Grnd. | Conduit | $\begin{array}{\|l\|} \hline \text { X-FMR } \\ (\mathrm{kVA}) \end{array}$ | X-Prim Prot | $\begin{array}{\|l} \hline \text { X-Sec } \\ \text { Prot } \\ \hline \end{array}$ | Primary Feeder | Primary Ground |
| RP-BN | 35.1 | 98 | 112.1 | 125 | 225 | (4) \#1 | \#6 | 1-1/4" EMT |  |  |  |  |  |
| RP-1NA | 27.1 | 75 | 86.4 | 90 | 100 | (4) \#3 | \#8 | 1-1/4" EMT |  |  |  |  |  |
| RP-1NB | 33.9 | 94 | 108.3 | 110 | 225 | (4) \#2 | \#6 | 1-1/4" EMT |  |  |  |  |  |
| RP-2NA | 17.4 | 48 | 55.5 | 60 | 100 | (4) \#6 | \#10 | 3/4" EMT |  |  |  |  |  |
| RP-2NB | 26.4 | 73 | 84.3 | 90 | 100 | (4) \#3 | \#8 | 1-1/4" EMT |  |  |  |  |  |
| RP-3NA | 29.6 | 82 | 94.4 | 100 | 100 | (4) \#3 | \#8 | 1-1/4" EMT |  |  |  |  |  |
| RP-3NB | 31.7 | 88 | 101.2 | 110 | 225 | (4) \#2 | \#6 | 1-1/4" EMT |  | 302 | 698 |  |  |
| Total | 201 | 558 | 642 | 700 | 800 | 2 sets (4) 350MCM | 1/0 | (2) 2-1/2" EMT | 225 | 300 | 700 | (3) 350MCM | \#4 |

Figure 3.4.3 - Design Calculation for DR-1

| DR-2 <br> Redesign Equipment Sizing |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL | kVA | Amps | Amps (growth) | Brk. | Bus | Feeder (THWN) | Grnd. | Conduit | $\begin{aligned} & \mathrm{X}-\mathrm{FMR} \\ & (\mathrm{kVA}) \end{aligned}$ | X-Prim <br> Prot | $\overline{X-S e c}$ Prot | Primary Feeder | Primary Ground |
| RP-1SA-1 | 31.8 | 88 | 101.6 | 90 | 225 |  |  |  |  |  |  |  |  |
| RP-1SA-2 | 42.2 | 117 | 134.8 | 125 | 225 |  |  |  |  |  |  |  |  |
| RP-1SA-3 | 50.6 | 141 | 161.7 | 150 | 225 |  |  |  |  |  |  |  |  |
| SubTotal | 124.7 | 346.1 |  | 350 |  | (4) 500MCM | \#3 | 3" EMT |  |  |  |  |  |
| RP-2SA-1 | 28.7 | 80 | 91.5 | 80 | 225 |  |  |  |  |  |  |  |  |
| RP-2SA-2 | 38.8 | 108 | 123.9 | 110 | 225 |  |  |  |  |  |  |  |  |
| RP-2SA-3 | 41.3 | 115 | 131.8 | 125 | 225 |  |  |  |  |  |  |  |  |
| SubTotal | 108.8 | 302.0 |  | 350 |  | (4) 350 MCM | \#3 | 2-1/2" EMT |  |  |  |  |  |
| RP-3SA-1 | 36.5 | 101 | 116.5 | 110 | 225 |  |  |  |  |  |  |  |  |
| RP-3SA-2 | 48.7 | 135 | 155.3 | 150 | 225 |  |  |  |  |  |  |  |  |
| RP-3SA-3 | 38.1 | 106 | 121.5 | 110 | 225 |  |  |  |  | 887 | 2048 |  |  |
| SubTotal | 123.2 | 342.0 |  | 350 |  | (4) 500 MCM | \#3 | 3"EMT |  |  |  |  |  |
| Total | 590 | 1638 | 1139 | 1200 | 1200 | 3 sets (4) 500MCM | 3/0 | (3) 3" EMT | 500 | 600 | 1200 | 2 Sets (3) 350MCM | \#1 |

## Figure 3.4.4 - Design Calculation for DR-2

*Note: Growth was not used in this calculation because the panels are completely full. There is not physical room for growth.

| DR-3Redesign Equipment Sizing |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL | kVA | Amps | Amps (growth) | Brk. | Bus | Feeder (THWN) | Grnd. |  | $\begin{array}{\|l\|} \hline \begin{array}{l} \text { X-FMR } \\ (k V A) \end{array} \\ \hline \end{array}$ | X-Prim <br> Prot | $\begin{aligned} & \text { X-Sec } \\ & \text { Prot } \end{aligned}$ | Primary Feeder | Primary Ground |
| RP-BS | 33.2 | 92 | 105.8 | 110 | 225 | (4) \#2 | \#6 | 1-1/4" EMT |  |  |  |  |  |
| RP-BSA | 35.9 | 100 | 114.7 | 125 | 225 | (4) \#1 | \#6 | 1-1/4" EMT |  |  |  |  |  |
| RP-1SB | 41.3 | 115 | 132.0 | 150 | 225 | (4) $1 / 0$ | \#6 | 1-1/2" EMT |  |  |  |  |  |
| RP-2SB | 30.0 | 83 | 95.7 | 100 | 100 | (4) \#3 | \#8 | 1-1/4" EMT |  |  |  |  |  |
| RP-3SB | 51.0 | 141 | 162.7 | 175 | 225 | (4) $2 / 0$ | \#6 | 2' EMT |  | 288 | 664 |  |  |
| Total | 191 | 531 | 611 | 700 | 800 | 2 sets (4) 350MCM | 1/0 | (2) 2-1/2" EMT | 225 | 300 |  | (3) 350MCM | \#4 |

Figure 3.4.5 - Design Calculation for DR-3

## Redesign System Schedules

| REDESIGN TRANSFORMER SCHEDULE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TAG | PRIMARY VOLTAGE | $\begin{aligned} & \hline \text { SECONDARY } \\ & \text { VOLTAGE } \\ & \hline \end{aligned}$ | SIZE | TYPE | $\begin{gathered} \hline \text { TEMP. } \\ \text { RISE } \end{gathered}$ | TAPS | MOUNTING |
| XD-1 | 13.2kV, 3P, 3W | 480Y/277V, 3P, 4W | 1500kVA | Silicone-based dielectric filled | $55^{\circ} \mathrm{C}$ | (4) $2.5 \%$ Taps <br> (2) Up \& (2) Dn | Concrete Pad Mount (outside) |
| XS-5 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) 2.5\% Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |
| XS-10 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |
| XS-11 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |
| XS-12 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 225kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |
| XS-13 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 300kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |
| XS-14 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 225kVA | Dry Type | $115{ }^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |

## Figure 3.5.1 - Redesign Distribution System Transformer Schedule

| REDESIGN FEEDER SCHEDULE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TAG | FROM | TO | NO. OF SETS | CONDUIT (PER SET) |  | PHASE CONDUCTORS |  | CONDUCTORS (PER SET) |  |  |  | GROUND CONDUCTORS |  |  | $\qquad$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SIZE | TYPE | No. | SIZE | TYPE | No. | SIZE | TYPE | No. | SIZE | TYPE |  |
| 1 | UTILITY | XD-1 | 1 | $4{ }^{\prime \prime}$ | PVC | 3 | 4/0 | -- | -- | -- | -- | 1 | 2 | -- | --- |
| 2 | UTILITY | XD-1 | 1 | 4" | PVC | 3 | 4/0 | -- | -- | -- | -- | 1 | 2 | -- | -- |
| 3 | XD-1 | MDB | 7 | 4 " | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 350 | CU THWN | --- |
| 4 | XD-1 | FP | 1 | 1.5 " | EMT | 3 | 1/0 | CU THWN | 1 | 3 | CU THWN | 1 | 6 | CU THWN | -- |
| 5 | Disc. Sw | Fire Pump | 1 | 1.5" | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 800A Fuse |
| 24 | MDB | XS-5 | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 225A, 3P |
| 25 | XS-5 | $\begin{gathered} \text { RP-K } \\ (\text { Sec.1) } \end{gathered}$ | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 150A, 3P |
| 26 | $\begin{gathered} \text { RP-K } \\ (\text { Sec. 1) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { RP-K } \\ \text { (Sec.2) } \end{gathered}$ | 1 | 2.5 | EMT | 3 | 250 | CU THWN | 1 | 250 | CU THWN | 1 | 4 | CU THWN | 150A, 3P |
| 35 | MDB | ELEV. | 1 | 2 | EMT | 3 | 3/0 | CU THWN | 1 | 3/0 | CU THWN | 1 | 6 | CU THWN | 800A Fuse |
| 36 | MDB | Elev-BN | 1 | 3 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 49 | MDB | Snow Mlt. | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 50 | MDB | ATS-LS | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 51 | ATS-LS | GEN | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 52 | ATS-LS | EDP-BS | 1 | $2 . .5$ | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 400A, 3P |
| 53 | EDP-BS | XS-10 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 54 | XS-10 | ERP-BS | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 100A, 3P |
| 55 | ERP-BS | ERP-1S | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 60A, 3P |
| 56 | ERP-1S | ERP-3S | 1 | 1.25 | EMT | 3 | 4 | CU THWN | , | 4 | CU THWN | 1 | 8 | CU THWN | 50A, 3P |
| 57 | EDP-BS | ELP-1S | 1 | 1.5 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 50A, 3P |
| 58 | ELP-3S | ELP-3S | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 59 | EDP-BS | ELP-1N | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 60 | ELP-1N | ELP-3N | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 61 | EDP-BS | ELP-BS | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 62 | MDB | MCC | 2 | 3 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 1 | CU THWN | 750A, 3P |
| 63 | MDB | DP-PH | 1 | 2.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 4 | CU THWN | 225A, 3P |
| 64 | MDB | ATS-NLS | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 65 | ATS-NLS | GEN | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 70A, 3P |
| 66 | ATS-NLS | ENDPH-BS | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 67 | ENDPH-BS | XS-11 | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 0 | -- | CU THWN | 1 | 8 | CU THWN | 125A, 3P |
| 68 | XS-11 | ENDPL-BS | 1 | 2 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 250A, 3P |
| 69 | ENDPL-BS | ENP-MDF | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 70 | ENDPL-BS | ENP-MDF2 | 1 | 1.5 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 71 | ENDPL-BS | ENP-BS | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 72 | ENDPL-BS | ENP-1S | 1 | 1.25 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 73 | ENP-1S | ENP-3S | 1 | 1 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 74 | MDB | DL-1 | 1 | 2.5 | EMT | 3 | 300 | CU THWN | 1 | 300 | CU THWN | 1 | 4 | CU THWN | 300A, 3P |
| 75 | DL-1 | LP-BN | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 90A, 3P |
| 76 | DL-1 | LP-1N | 1 | 0.75 | EMT | 3 | 8 | CU THWN | 1 | 8 | CU THWN | 1 | 10 | CU THWN | 50A, 3P |
| 77 | DL-1 | LP-2N | 1 | 0.75 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 78 | DL-1 | LP-3N | 1 | 1 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 80A, 3P |
| 79 | MDB | DL-2 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 400A, 3P |
| 80 | DL-2 | LP-BS | 1 | 1.5 | EMT | 3 | 4/0 | CU THWN | 1 | 4/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 81 | DL-2 | LP-1S | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 90A, 3P |
| 82 | DL-2 | LP-2S | 1 | 1 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 80A, 3P |
| 83 | DL-2 | LP-3S | 1 | 1 | EMT | 3 | 4 | CU THWN | 1 | 4 | CU THWN | 1 | 8 | CU THWN | 80A, 3P |
| 84 | MDB | XS-2 | 1 | 2.5 | EMT | 3 | 350 | CU THWN | 0 | -- | CU THWN | 1 | 4 | CU THWN | 300A, 3P |
| 85 | XS-3 | DR-1 | 2 | 2.5 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 1/0 | CU THWN | 700A, 3P |
| 86 | DR-1 | RP-BN | 1 | 1.25 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 87 | DR-1 | RP-1NA | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 90A, 3P |
| 88 | DR-1 | RP-1NB | 1 | 1.25 | EMT | 3 | 2 | CU THWN | 1 | 2 | CU THWN | 1 | 6 | CU THWN | 110A, 3P |
| 89 | DR-1 | RP-2NA | 1 | 0.75 | EMT | 3 | 6 | CU THWN | 1 | 6 | CU THWN | 1 | 10 | CU THWN | 60A, 3P |
| 90 | DR-1 | RP-2NB | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 90A, 3P |
| 91 | DR-1 | RP-3NA | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 92 | DR-1 | RP-3NB | 1 | 1.25 | EMT | 3 | 2 | CU THWN | 1 | 2 | CU THWN | 1 | 6 | CU THWN | 110A, 3P |
| 93 | MDB | XS-3 | 2 | 2.5 | EMT | 3 | 350 | CU THWN | 0 | -- | CU THWN | 1 | 1 | CU THWN | 600A, 3P |
| 94 | XS-3 | DR-2 | 3 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3/0 | CU THWN | 1200A, 3P |
| 95 | DR-2 | RP-1SA-1 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 96 | RP-1SA-1 | RP-1SA-2 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 97 | RP-1SA-2 | RP-1SA-3 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 98 | DR-2 | RP-2SA-1 | 1 | 2.5 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 99 | RP-2SA-1 | RP-2SA-2 | 1 | 2.5 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 100 | RP-2SA-2 | RP-2SA-3 | 1 | 2.5 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 101 | DR-2 | RP-3SA-1 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 102 | RP-3SA-1 | RP-3SA-2 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 103 | RP-3SA-2 | RP-3SA-3 | 1 | 3 | EMT | 3 | 500 | CU THWN | 1 | 500 | CU THWN | 1 | 3 | CU THWN | 350A, 3P |
| 104 | MDB | XS-4 | 1 | 2.5 | EMT | 3 | 350 | CU THWN | 0 | -- | CU THWN | 1 | 4 | CU THWN | 300A, 3P |
| 105 | XS-4 | DR-3 | 2 | 2.5 | EMT | 3 | 350 | CU THWN | 1 | 350 | CU THWN | 1 | 1/0 | CU THWN | 700A, 3P |
| 106 | DR-3 | RP-BS | 1 | 1.25 | EMT | 3 | 2 | CU THWN | 1 | 2 | CU THWN | 1 | 6 | CU THWN | 110A, 3P |
| 107 | DR-3 | RP-BSA | 1 | 1.25 | EMT | 3 | 1 | CU THWN | 1 | 1 | CU THWN | 1 | 6 | CU THWN | 125A, 3P |
| 108 | DR-3 | RP-1SB | 1 | 1.5 | EMT | 3 | 1/0 | CU THWN | 1 | 1/0 | CU THWN | 1 | 6 | CU THWN | 150A, 3P |
| 109 | DR-3 | RP-2SB | 1 | 1.25 | EMT | 3 | 3 | CU THWN | 1 | 3 | CU THWN | 1 | 8 | CU THWN | 100A, 3P |
| 110 | DR-3 | RP-3SB | 1 | 2 | EMT | 3 | 2/0 | CU THWN | 1 | 2/0 | CU THWN | 1 | 6 | CU THWN | 175A, 3P |

Figure 3.5.2 - Redesign Distribution System Feeder Schedule

## Redesign Panel Board Schedules



Figure 3.6.1 - LP-1N Redesign Panelboard Schedule


Figure 3.6.2 - RP-1NA Redesign Panelboard Schedule


Figure 3.6.3 - LP-2N Redesign Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: RP-2NA | EQUIP. GND. BUS: |  |  |  |  |  | VOLTAGE: |  |  | $120 / 208$ VOLT, 3PH, 4W |
| LOCATION: $\quad$ ELEC.RM.(266)-2ND FL. | ISOLATED GND BUS: |  |  |  |  | 200\% | MAIN CIRCUIT BKR: |  |  | R: 150 |
| MOUNTING: SURFACE | NEUTRAL BUS: |  |  | 100\% |  |  | $\square$ | MLO: |  | 100 |
| FED FROM: PANEL 'LP-2N' |  | A.l.C.: | 22000 |  |  |  |  | BUS RA | ING: |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 1 | 720 |  |  |  |  |  | 260B/264 RECEPTACLES |
|  |  |  |  | 1.080 |  |  | 2 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 3 |  | 720 |  |  |  |  | 264 WALL QUAD RECEPTACLES (COMP) |
|  |  |  |  |  | 720 |  | 4 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 264 WALL QUAD RECEPTACLES (COMP) |
|  |  |  |  |  |  | 720 | 6 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 7 | 720 |  |  |  |  |  | 264 WALL QUAD RECEPTACLES (COMP) |
|  |  |  |  | 720 |  |  | 8 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | 264 WALL QUAD RECEPTACLES (COMP) |
|  |  |  |  |  | 720 |  | 10 | 1 | 20 |  |
| 265 COMP. WALL RECEPTACLES | 20 | 1 | 11 |  |  | 720 |  |  |  | 264 GEN RECEPTACLES |
|  |  |  |  |  |  | 900 | 12 | 1 | 20 |  |
| 260B/265 RECEPTACLES | 20 | 1 | 13 | 720 |  |  |  |  |  | 260 WALL QUAD RECEPTACLES |
|  |  |  |  | 720 |  |  | 14 | 1 | 20 |  |
| 267 GENERAL RECEPTACLES | 20 | 1 | 15 |  | 360 |  |  |  |  | 260A EWC RECEPTACLE |
|  |  |  |  |  | 500 |  | 16 | 1 | 20 |  |
| 260B JUNCTION BOX | 20 | 1 | 17 |  |  | 1,000 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 18 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 19 | 720 |  |  |  |  |  | TF-2-1 |
|  |  |  |  | 506 |  |  | 20 | 1 | 15 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 21 |  | 720 |  |  |  |  | FP-2-3 |
|  |  |  |  |  | 830 |  | 22 | 1 | 15 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 23 |  |  | 720 |  |  |  | UH-1 |
|  |  |  |  |  |  | 506 | 24 | 1 | 15 |  |
| 265 WALL RECEPTACLES | 20 | 1 | 25 | 540 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 26 | 1 | 20 |  |
| 265 FLOOR QUAD RECEPTACLES | 20 | 1 | 27 |  | 360 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| SPARE | 20 | 1 | 29 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 30 | 1 | 20 |  |
| SPARE | 20 | 1 | 31 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 32 | 1 | 20 |  |
| SPARE | 20 | 1 | 33 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 34 | 1 | 20 |  |
| SPARE | 20 | 1 | 35 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 36 | 1 | 20 |  |
| SPARE | 20 | 1 | 37 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 38 | 3 | 100 |  |
| SPARE | 20 | 1 | 39 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 40 |  |  |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 42 |  |  |  |
|  | TOTAL VA |  |  | , 446 | 5,650 | 5,286 | TOTAL KVA |  |  | 17.382 |
|  | TOTAL AMP/PHASE |  |  | 54 | 47 | 44 | TOTAL AMP |  |  | 48 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.6.4 - RP-2NA Redesign Panelboard Schedule


Figure 3.6.5 - LP-3N Redesign Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PANEL: RP-3NA | EQUIP. GND. BUS: |  |  |  | $\square$ | 200\% | VOLTAGE: |  |  | $120 / 208$ VOLT, 3PH, 4W |
| ELEC.RM.(366)-3RD FL. |  | ISOLAT | D GND |  |  |  | MAIN CIRCUIT BKR: |  |  | 100A |
| MOUNTING: $\qquad$ | NEUTRAL BUS: |  |  | 100\% |  |  |  | MLO: |  |  |
| FED FROM: PANEL 'LP-3N' |  | A.I.C.: |  | 22,000 |  |  |  | BUS RA | ING: |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | BKR. AMPS | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 365 RECEPTACLES | 20 | 1 | 1 | 360 |  |  |  |  |  | ROOF RECEPTACLES |
|  |  |  |  | 360 |  |  | 2 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 3 |  | 360 |  |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  | 1.440 |  | 4 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 367 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 6 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 7 | 720 |  |  |  |  |  | 360B RECEPTACLES |
|  |  |  |  | 1.260 |  |  | 8 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | 360 RECEPTACLES |
|  |  |  |  |  | 1.440 |  | 10 | 1 | 20 |  |
| 370/371 RECEPTACLES | 20 | 1 | 11 |  |  | 1,260 |  |  |  | 372 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 12 | 1 | 20 |  |
| 370 RECEPTACLES | 20 | 1 | 13 | 1,080 |  |  |  |  |  | 368 RECEPTACLES \& DOOR HOLDERS |
|  |  |  |  | 1.460 |  |  | 14 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 15 |  | 720 |  |  |  |  | FP-3-4 |
|  |  |  |  |  | 800 |  | 16 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 17 |  |  | 720 |  |  |  | TE-3-1 |
|  |  |  |  |  |  | 299 | 18 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 19 | 720 |  |  |  |  |  | TF-3-1 |
|  |  |  |  | 500 |  |  | 20 | 1 | 15 |  |
| 364 RECEPTACLES | 20 | 1 | 21 |  | 720 |  |  |  |  | FP-3-3 |
|  |  |  |  |  | 830 |  | 22 | 1 | 15 |  |
| 374 RECEPTACLES | 20 | 1 | 23 |  |  | 720 |  |  |  | UH-1 |
|  |  |  |  |  |  | 506 | 24 | 1 | 15 |  |
| 376 COPIER | 20 | 1 | 25 | 1,000 |  |  |  |  |  | J-BOX, VAV |
|  |  |  |  | 1,000 |  |  | 26 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 27 |  | 900 |  |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  | 720 |  | 28 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 29 |  |  | 720 |  |  |  | 365 RECEPTACLES |
|  |  |  |  |  |  | 720 | 30 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 31 | 720 |  |  |  |  |  | LIGHTING 365 PENDANTS |
|  |  |  |  | 322 |  |  | 32 | 1 | 20 |  |
| 360 RECEPTACLES | 20 | 1 | 33 |  | 900 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 34 | 1 | 20 |  |
| 375 RECEPTACLES | 20 | 1 | 35 |  |  | 540 |  |  |  | SPARE |
|  |  |  |  |  |  |  | 36 | 1 | 20 |  |
| 365 RECEPTACLES | 20 | 1 | 37 | 720 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 38 | 3 | 50 |  |
| 365 RECEPTACLES | 20 | 1 | 39 |  | 720 |  |  |  |  |  |
|  |  |  |  |  |  |  | 40 |  |  |  |
| SPARE | 20 | 1 | 41 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 42 |  |  |  |
|  | TOTAL VA |  |  | 10.222 | 10.270 | 9,085 | TOTAL KVA |  |  | 29.577 |
|  | TOTAL | AMP/PH |  | 85 | 86 | 76 | TOTAL | AMP |  | 82 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.6.6 - RP-3NA Redesign Panelboard Schedule


Figure 3.6.7 - LP-1S Redesign Panelboard Schedule


Figure 3.6.8 - RP-1SA-1 Redesign Panelboard Schedule


Figure 3.6.9 -LP-BN Redesign Panelboard Schedule


Figure 3.6.10 - LP-BS Redesign Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RP-BS |  | EQUIP. GND. BUS: $\quad \square$ |  |  |  |  |  | VOLTAGE: |  | $120 / 208$ VOLT, 3PH, 4W |
| ELEC.RM (B02)-SUB.BSMT |  | ISOLATED GND BUS: |  |  |  | 200\% |  | MAIN CIRCUIT BKR |  | R: 200 |
| SURFACE |  | NEUTRAL BUS: |  | 100\% | $\square$ |  |  | MLO: $\quad \square$ |  | 100 |
| FED FROM: PANEL 'LP-BS' |  | A.I.C.: | 10000 |  |  |  |  | BUS RA | NG: |  |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \\ & \hline \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| L11 GENERAL RECEPTACLES | 20 | 1 | 1 | 360 |  |  |  |  |  | L13A/L14/L15A/OUTDOOR RECEPTACLES |
|  |  |  |  | 1.260 |  |  | 2 | 1 | 20 |  |
| L12 PRINTER RECEPTACLE | 20 | 1 | 3 |  | 1,000 |  |  |  |  | L14 COFF. RECEPTACLE |
|  |  |  |  |  | 720 |  | 4 | 1 | 20 |  |
| L10 RECPTACLES | 20 | 1 | 5 |  |  | 540 |  |  |  | L14 MICR. RECEPTACLE |
|  |  |  |  |  |  | 750 | 6 | 1 | 20 |  |
| L10 RECEPTACLES | 20 | 1 | 7 | 720 |  |  |  |  |  | L14 REF RECEPTACLE |
|  |  |  |  | 750 |  |  | 8 | 1 | 20 |  |
| L10 RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | L10/S2-L RECEPTACLES |
|  |  |  |  |  | 360 |  | 10 | 1 | 20 |  |
| L13 RECEPTACLES | 20 | 1 | 11 |  |  | 900 |  |  |  | B02,A GENERAL RECEPTACLES <br> \& MOTORIZED DAMPERS |
|  |  |  |  |  |  | 900 | 12 | 1 | 20 |  |
| L13A RECEPTACLES | 20 | 1 | 13 | 900 |  |  |  |  |  | EUH-2 |
|  |  |  |  | 1.650 |  |  | 14 | 2 | 20 |  |
| L13 RECEPTACLES | 20 | 1 | 15 |  | 720 |  |  |  |  |  |
|  |  |  |  |  | 1,650 |  | 16 |  |  |  |
| L13 RECEPTACLES | 20 | 1 | 17 |  |  | 720 |  |  |  | EUH-1 |
|  |  |  |  |  |  | 1.650 | 18 | 2 | 20 |  |
| L09A, B/L13,A RECEPTACLESAUTO SENSORS | 20 | 1 | 19 | 1,180 |  |  |  |  |  |  |
|  |  |  |  | 1.650 |  |  | 20 |  |  |  |
| L10 CORRIDOR EWC | 20 | 1 | 21 |  | 500 |  |  |  |  |  |
|  |  |  |  |  | 830 |  | 22 | 1 | 15 |  |
| SPARE | 20 | 1 | 23 |  |  |  |  |  |  | UH-1 |
|  |  |  |  |  |  | 506 | 24 | 1 | 15 |  |
| L12 J1 | 20 | 1 | 25 | 1,500 |  |  |  |  |  | LIGHTING <br> DINING/KICHEN HALOGEN |
|  |  |  |  | 200 |  |  | 26 | 1 | 20 |  |
| L13 AV | 20 | 1 | 27 |  | 1,100 |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 28 | 1 | 20 |  |
| 103 PS | 20 | 1 | 29 |  |  | 1,400 |  |  |  | 102 J 2 |
|  |  |  |  |  |  | 1.500 | 30 | 1 | 20 |  |
| 103 J 2 | 20 | 1 | 31 | 1,500 |  |  |  |  |  | 102 PS |
|  |  |  |  | 1.400 |  |  | 32 | 1 | 20 |  |
| 103 F 2 | 20 | 1 | 33 |  | 750 |  |  |  |  | 102 F 2 |
|  |  |  |  |  | 750 |  | 34 | 1 | 20 |  |
| 103 F 2 | 20 | 1 | 35 |  |  | 750 |  |  |  | 102 VP |
|  |  |  |  |  |  | 435 | 36 | 1 | 20 |  |
| SPARE |  |  | 37 |  |  |  |  |  |  | LIGHTING (FUTURE) DRIVEWAY SIGN |
|  |  |  |  | 200 |  |  | 38 | 1 | 20 |  |
|  | 100 | 3 | 39 |  |  |  |  |  |  | MOTORIZED DOORS (L10, L10A, L13B) \& MAGLOCKS (L13B, L13C) |
|  |  |  |  |  | 732 |  | 40 | 1 | 20 |  |
|  |  |  | 41 |  |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 42 | 1 | 20 |  |
|  | TOTAL VA |  |  | 3.270 | 9,832 | 0.051 | TOTAL KVA |  |  | 33.2 |
|  | TOTAL | AMP/PH |  | 111 | 82 | 84 | TOTAL AMP |  |  | 92 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.6.11 - RP-BS Redesign Panelboard Schedule


Figure 3.6.12 - LP-2S Redesign Panelboard Schedule


Figure 3.6.13 - RP-2SA-1 Redesign Panelboard Schedule


Figure 3.6.14 - LP-3S Redesign Panelboard Schedule

| PANELBOARD SCHEDULE |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RP-3SA-1 |  |  |  |  |  | $\square$ |  | VOLTAGE: |  | 120/208 VOLT, 3PH, 4W |
| ELEC.RM.(319A)-3RD FL. |  | ISOLATED GND BUS: |  |  |  | 200\% |  | MAIN CIRCUIT BKR: |  | 125 |
| SURFACE |  | NEUTRAL BUS: |  |  |  |  |  | MLO: |  |  |
| FED FROM: PANEL 'LP-3S' |  | A.I.C.: | 22000 |  |  |  |  | BUS RA | ING: | 225 |
| LOAD DESCRIPTION | $\begin{gathered} \hline \text { BKR. } \\ \text { AMPS } \end{gathered}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | $\begin{aligned} & \hline \text { CKT. } \\ & \text { NO. } \end{aligned}$ | LOAD - V.A. |  |  | $\begin{aligned} & \text { CKT. } \\ & \text { NO. } \end{aligned}$ | $\begin{aligned} & \hline \text { BKR. } \\ & \text { POLE } \end{aligned}$ | BKR. AMPS | LOAD DESCRIPTION |
|  |  |  |  | A | B | C |  |  |  |  |
| 360 RECEPTACLES | 20 | 1 | 1 | 720 |  |  |  |  |  | J-BOX, VAV |
|  |  |  |  | 1.000 |  |  | 2 | 1 | 20 |  |
| 362 RECEPTACLES | 20 | 1 | 3 |  | 720 |  |  |  |  | 350 RECEPTACLES |
|  |  |  |  |  | 1,340 |  | 4 | 1 | 20 |  |
| 363 RECEPTACLES | 20 | 1 | 5 |  |  | 720 |  |  |  | 318B RECEPTACLES |
|  |  |  |  |  |  | 1.340 | 6 | 1 | 20 |  |
| 349 RECEPTACLES | 20 | 1 | 7 | 720 |  |  |  |  |  | 339 RECEPTACLES |
|  |  |  |  | 1,440 |  |  | 8 | 1 | 20 |  |
| 349 RECEPTACLES | 20 | 1 | 9 |  | 720 |  |  |  |  | 337 RECEPTACLES |
|  |  |  |  |  | 1.440 |  | 10 | 1 | 20 |  |
| 340 RECEPTACLES | 20 | 1 | 11 |  |  | 720 |  |  |  | GE-R-1 |
|  |  |  |  |  |  | 506 | 12 | 1 | 15 |  |
| 340 RECEPTACLES | 20 | 1 | 13 | 720 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 14 | 1 | 15 |  |
| 337 RECEPTACLES | 20 | 1 | 15 |  | 720 |  |  |  |  | TE-R-2 |
|  |  |  |  |  | 830 |  | 16 | 1 | 15 |  |
| 335 RECEPTACLES | 20 | 1 | 17 |  |  | 720 |  |  |  | CE-R-2 |
|  |  |  |  |  |  | 506 | 18 | 1 | 15 |  |
| 333 RECEPTACLES | 20 | 1 | 19 | 720 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 20 | 1 | 20 |  |
| 331 RECEPTACLES | 20 | 1 | 21 |  | 720 |  |  |  |  | 334 RECEPTACLES |
|  |  |  |  |  | 1,440 |  | 22 | 1 | 20 |  |
| 329 RECEPTACLES | 20 | 1 | 23 |  |  | 720 |  |  |  | 332 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 24 | 1 | 20 |  |
| 327 RECEPTACLES | 20 | 1 | 25 | 720 |  |  |  |  |  | J-BOX, VAV |
|  |  |  |  | 1,000 |  |  | 26 | 1 | 20 |  |
| 324 RECEPTACLES | 20 | 1 | 27 |  | 720 |  |  |  |  | 326 RECEPTACLES |
|  |  |  |  |  | 1.440 |  | 28 | 1 | 20 |  |
| 322 COPIER | 20 | 1 | 29 |  |  | 1,000 |  |  |  | 323 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 30 | 1 | 20 |  |
| 321 RECEPTACLES | 20 | 1 | 31 | 1,080 |  |  |  |  |  | 321 RECEPTACLES |
|  |  |  |  | 1.440 |  |  | 32 | 1 | 20 |  |
| 321 RECEPTACLES | 20 | 1 | 33 |  | 360 |  |  |  |  | 302 RECEPTACLES |
|  |  |  |  |  | 1.440 |  | 34 | 1 | 20 |  |
| 323 RECEPTACLES | 20 | 1 | 35 |  |  | 360 |  |  |  | 302 RECEPTACLES |
|  |  |  |  |  |  | 1.440 | 36 | 1 | 20 |  |
| 302 RECEPTACLES | 20 | 1 | 37 | 1,440 |  |  |  |  |  | SPARE |
|  |  |  |  |  |  |  | 38 | 3 | 100 |  |
| 302 RECEPTACLES | 20 | 1 | 39 |  | 1,440 |  |  |  |  |  |
|  |  |  |  |  |  |  | 40 |  |  |  |
| 327/328/329 GENERAL RECEPTS | 20 | 1 | 41 |  |  | 1,260 |  |  |  |  |
|  |  |  |  |  |  |  | 42 |  |  |  |
|  | TOTAL VA |  |  | 11.000 | 13.330 | 12.172 | TOTAL KVA |  |  | 36.5 |
|  | TOTAL | AMP/PH |  | 92 | 111 | 101 | TOTAL | AMP |  | 101 |
| REMARKS: |  |  |  |  |  |  |  |  |  |  |

Figure 3.6.15 - RP-3SA-1 Redesign Panelboard Schedule


Figure 3.7.1 - Redesign Distribution System Single Line
*See Appendix D for full size single line

## Cost Analysis

| LP-1NEquipment Cost of Original System |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of <br> Feeders | Feeder Length (CFL) | Per Unit Cost | Cost |
| 400A, 3P Breaker (480) | 0430 | N/A | N/A | \$2,780.00 | \$2,780.00 |
| 2 Sets (4)1/0, \#3G, (2) 2" EMT | 1600 | 8 | 4 | \$344.00 | \$11,008.00 |
| LP-1N (400A) | 3230 | N/A | N/A | \$1,455.00 | \$1,455.00 |
| 125A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (3) 1/0, \#6G, 1.5 EMT | 1600 | 3 | 0.25 | \$344.00 | \$258.00 |
| 75 kVA X -Fmr | 4915 | N/A | N/A | \$7,000.00 | \$7,000.00 |
| (4) $250 \mathrm{MCM}, \# 4 \mathrm{G}, 2.5 \mathrm{EMT}$ | 2200 | 4 | 0.25 | \$727.00 | \$727.00 |
| 250A, 3P Breaker (208) | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| RP-1NA (400A) | 3130 | N/A | N/A | \$1,245.00 | \$1,245.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 0.25 | \$286.00 | \$286.00 |
| RP-1NB (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 150A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) 1/0, \#6G, 2 EMT | 1600 | 4 | 0.25 | \$344.00 | \$344.00 |
| LP-2N (225) | 3220 | N/A | N/A | \$1,045.00 | \$1,045.00 |
| 70A, 3P Breaker (480) | 0370 | N/A | N/A | \$606.00 | \$606.00 |
| (3) \#4, \#8G, 1.25 EMT | 1400 | 3 | 0.25 | \$166.50 | \$124.88 |
| 45 kVA X -Fmr | 4910 | N/A | N/A | \$5,110.00 | \$5,110.00 |
| (4) 1/0, \#6G, 2 EMT | 1600 | 4 | 0.25 | \$344.00 | \$344.00 |
| 150A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-2NA (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 2.5 | \$286.00 | \$2,860.00 |
| RP-2NB (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 150A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) 1/0, \#6G, 2 EMT | 1600 | 4 | 0.5 | \$344.00 | \$688.00 |
| LP-3N (225A) | 3220 | N/A | N/A | \$1,045.00 | \$1,045.00 |
| 70A, 3P Breaker (480) | 0370 | N/A | N/A | \$606.00 | \$606.00 |
| (3) \#4, \#8G, 1.25 EMT | 1400 | 3 | 0.25 | \$166.50 | \$124.88 |
| 45 kVA X -Fmr | 4910 | N/A | N/A | \$5,110.00 | \$5,110.00 |
| (4) 1/0, \#6G, 2 EMT | 1600 | 4 | 0.25 | \$344.00 | \$344.00 |
| 150A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-2NA (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 50A, 3P Breaker (208) | 0180 | N/A | N/A | \$365.00 | \$365.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 2.5 | \$286.00 | \$2,860.00 |
| RP-3NB (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
|  |  |  |  | Total | \$60,079.75 |

Figure 3.8.1 - Original Cost Information for LP-1N Panel

| LP-1SEquipment Cost of Original System |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | $\begin{aligned} & \text { Feeder } \\ & \text { Length (CFL) } \\ & \hline \end{aligned}$ | Per Unit Cost | Cost |
| 400A, 3P Breaker (480) | 0430 | N/A | N/A | \$2,780.00 | \$2,780.00 |
| (4)350MCM, \#4G, 3 EMT | 2600 | 4 | 2.5 | \$967.00 | \$9,670.00 |
| LP-1S (400A) | 3230 | N/A | N/A | \$1,455.00 | \$1,455.00 |
| 125A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (3) 1/0, \#6G, 1.5 EMT | 1600 | 3 | 0.25 | \$344.00 | \$258.00 |
| 112.5kVA X-Fmr | 4920 | N/A | N/A | \$13,439.00 | \$13,439.00 |
| (4) $250 \mathrm{MCM}, \# 4 \mathrm{G}, 2.5 \mathrm{EMT}$ | 2200 | 4 | 0.25 | \$727.00 | \$727.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-1SA-1 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) 250 MCM, \#4G, 2.5 EMT | 2200 | 4 | 2 | \$727.00 | \$5,816.00 |
| RP-1SB (225) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| (4) 250 MCM , \#4G, 2.5 EMT | 2200 | 4 | 0.25 | \$727.00 | \$727.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-1SA-2 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 0.25 | \$286.00 | \$286.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-1SA-3 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
|  |  |  |  | Total | \$44,390.00 |

Figure 3.8.2 - Original Cost Information for LP-1S Panel

| LP-BNEquipment Cost of Original System |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | $\begin{aligned} & \text { Feeder } \\ & \text { Length (CFL) } \end{aligned}$ | Per Unit Cost | Cost |
| 225A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4)4/0, \#4G, 2.5 EMT | 2000 | , | 3 | \$626.00 | \$7,512.00 |
| LP-BN (225A) | 3220 | N/A | N/A | \$1,045.00 | \$1,045.00 |
| 50A, 3P Breaker (480) | 0230 | N/A | N/A | \$499.00 | \$499.00 |
| (3) \#6, \#10G, 0.75 EMT | 1350 | 3 | 0.25 | \$118.00 | \$88.50 |
| 30 kVA X -Fmr | 4905 | N/A | N/A | \$4,385.00 | \$4,385.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 0.25 | \$286.00 | \$286.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| RP-BN (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| Total \$16,183.50 |  |  |  |  |  |

Figure 3.8.3 - Original Cost Information for LP-BN Panel

| LP-BSEquipment Cost of Original System |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | Feeder <br> Length (CFL) | Per Unit Cost | Cost |
| 225A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4)4/0, \#4G, 2.5 EMT | 2000 | 4 | 0.25 | \$626.00 | \$626.00 |
| LP-BS (225A) | 3220 | N/A | N/A | \$1,045.00 | \$1,045.00 |
| 225A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (3) 1/0, \#6G, 1.5 EMT | 1600 | 3 | 0.25 | \$344.00 | \$258.00 |
| 75kVA X-Fmr | 4915 | N/A | N/A | \$7,000.00 | \$7,000.00 |
| (4) 250MCM, \#4G, 2.5 EMT | 2200 | 4 | 0.25 | \$727.00 | \$727.00 |
| 400A, 3P Breaker (208) | 0430 | N/A | N/A | \$2,780.00 | \$2,780.00 |
| RP-BS (400A) | 3130 | N/A | N/A | \$1,245.00 | \$1,245.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) 250MCM, \#4G, 2.5 EMT | 2200 | 4 | 1.5 | \$727.00 | \$4,362.00 |
| RP-BSA (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| Total |  |  |  |  |  |
|  |  |  |  | Total | \$21,650.00 |

Figure 3.8.4 - Original Cost Information for LP-BS Panel


Figure 3.8.5 - Original Cost Information for LP-2S Panel

Jason Greer I Villanova University: School of Law

| LP-3SEquipment Cost of Original System |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | $\begin{aligned} & \text { Feeder } \\ & \text { Length (CFL) } \end{aligned}$ | Per Unit Cost | Cost |
| 225A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4)250MCM, \#4G, 2.5 EMT | 2200 | 4 | 3 | \$727.00 | \$8,724.00 |
| LP-3S (400A) | 3230 | N/A | N/A | \$1,455.00 | \$1,455.00 |
| 125A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (3) 1/0, \#6G, 1.5 EMT | 1600 | 3 | 0.25 | \$344.00 | \$258.00 |
| 112.5kVA X-Fmr | 4920 | N/A | N/A | \$13,439.00 | \$13,439.00 |
| (4) 3/0, \#6G, 2 EMT | 1700 | 4 | 0.25 | \$516.00 | \$516.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-3SA-1 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) 3/0, \#6G, 2 EMT | 1700 | 4 | 2 | \$516.00 | \$4,128.00 |
| RP-3SB (225) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| (4) 3/0, \#6G, 2 EMT | 1700 | 4 | 0.25 | \$516.00 | \$516.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-3SA-2 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| (4) \#1, \#8G, 1.5 EMT | 1550 | 4 | 0.25 | \$286.00 | \$286.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| RP-3SA-3 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
|  |  |  |  |  | \$39,793.00 |

Figure 3.8.6 - Original Cost Information for LP-3S Panel

| Original System |  |
| :---: | :---: |
| Total Original Cost | $\$ 220,281.25$ |

Figure 3.8.7 - Original Total Cost


Figure 3.8.8 - Redesign Cost Information for DL-1 Panel

| DL-2Equipment Costs for Redesign |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | Feeder <br> Length (CFL) | Per Unit Cost | Cost |
| 400A 3P, Breaker (480) | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (4) 500 MCM , \#3G, 3 EMT | 2800 | 4 | 0.25 | \$1,303.00 | \$1,303.00 |
| DL-2 Panel (400A) | 0190 | N/A | N/A | \$2,365.00 | \$2,365.00 |
| 150A, 3P Breaker (480) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) 1/0, \#6G, 1.5 EMT | 1600 | 4 | 0.25 | \$344.00 | \$344.00 |
| LP-BS (225A) | 3220 | N/A | N/A | \$1,045.00 | \$1,045.00 |
| 90A, 3P Breaker (480) | 0370 | N/A | N/A | \$606.00 | \$606.00 |
| (4) \#3, \#8G, 1.25 EMT | 1450 | 4 | 3 | \$196.00 | \$2,352.00 |
| LP-1S (100A) | 3210 | N/A | N/A | \$763.00 | \$763.00 |
| 80A, 3P Breaker (480) | 0370 | N/A | N/A | \$606.00 | \$606.00 |
| (4) \#4, \#8G, 1EMT | 1400 | 4 | 3.5 | \$166.50 | \$2,331.00 |
| LP-2S (100A) | 3210 | N/A | N/A | \$763.00 | \$763.00 |
| 80A, 3P Breaker (480) | 0370 | N/A | N/A | \$606.00 | \$606.00 |
| (4) \#4, \#8G, 1EMT | 1400 | 4 | 3.5 | \$166.50 | \$2,331.00 |
| LP-3S (100A) | 3210 | N/A | N/A | \$763.00 | \$763.00 |
|  |  |  |  | Total | \$20,125.00 |

Figure 3.8.9 - Redesign Cost Information for DL-2 Panel

| DR-1 <br> Equipment Costs for Redesign |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | $\begin{aligned} & \text { Feeder } \\ & \text { Length (CFL) } \end{aligned}$ | Per Unit Cost | Cost |
| 300A 3P, Breaker (480) | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (3) 350MCM, \#4G, 2.5 EMT | 2600 | 3 | 3 | 967 | \$8,703.00 |
| 225kVA X-Fmr | 4930 | N/A | N/A | \$23,374.00 | \$23,374.00 |
| 2 sets (4) 350MCM, 1/0G, (2) 2.5 EMT | 2600 | 8 | 0.25 | \$967.00 | \$1,934.00 |
| 700A, 3P Breaker (208) | 0470 | N/A | N/A | \$5,780.00 | \$5,780.00 |
| DR-1 Panel (800A) | 0300 | N/A | N/A | \$3,580.00 | \$3,580.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) \#1, \#6G, 1.25 EMT | 1550 | 4 | 0.25 | \$286.00 | \$286.00 |
| RP-BN (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 90A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#3, \#8G, 1.25 EMT | 1450 | 4 | 2.25 | \$196.00 | \$1,764.00 |
| RP-1NA (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 110A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) \#2, \#6G, 1.25 EMT | 1500 | 4 | 1.25 | \$235.00 | \$1,175.00 |
| RP-1NB (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 60A, 3P Breaker (208) | 0180 | N/A | N/A | \$365.00 | \$365.00 |
| (4) \#6, \#10G, 0.75 EMT | 1350 | 4 | 2.5 | \$118.00 | \$1,180.00 |
| RP-2NA (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 90A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#3, \#8G, 1.25 EMT | 1450 | 4 | 1.5 | \$196.00 | \$1,176.00 |
| RP-2NB (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#3, \#8G, 1.25 EMT | 1450 | 4 | 2.5 | \$196.00 | \$1,960.00 |
| RP-3NA (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 110A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) \#2, \#6G, 1.25 EMT | 1500 | 4 | 1.5 | \$235.00 | \$1,410.00 |
| RP-3NB (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
|  |  |  |  | Total | \$66,037.00 |

Figure 3.8.10 - Redesign Cost Information for DR-1 Panel

| DR-2 <br> Equipment Costs for Redesign |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | Feeder <br> Length (CFL) | Per Unit Cost | Cost |
| 600A, 3P Breaker (480) | 0460 | N/A | N/A | \$4,453.00 | \$4,453.00 |
| 2 sets (3) 350MCM, \#1G, (2) 2.5 EMT | 2600 | 6 | 3 | \$967.00 | \$17,406.00 |
| 500 kVA X-Fmr | 4940 | N/A | N/A | \$48,988.00 | \$48,988.00 |
| 3 sets (4) 500MCM, 3/0G, (3) 3 EMT | 2800 | 12 | 0.25 | \$1,303.00 | \$3,909.00 |
| 1200A, 3P Breaker (208) | 0500 | N/A | N/A | \$4,425.00 | \$4,425.00 |
| DR-2 Panel (1200A) | 0500 | N/A | N/A | \$4,425.00 | \$4,425.00 |
| 350A, 3P Breaker (208) | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (4) 500MCM, \#3G, 3 EMT | 2800 | 4 | 0.25 | \$1,303.00 | \$1,303.00 |
| RP-1SA-1 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-1SA-2 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-1SA-3 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 350A, 3P Breaker | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (4) $350 \mathrm{MCM}, \# 3 \mathrm{G}, 2.5 \mathrm{EMT}$ | 2600 | 4 | 0.5 | \$967.00 | \$1,934.00 |
| RP-2SA-1 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-2SA-2 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-2SA-3 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 350A, 3P Breaker | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (4) 500MCM, \#3G, 3 EMT | 2800 | 4 | 0.5 | \$1,303.00 | \$2,606.00 |
| RP-3SA-1 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-3SA-2 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| RP-3SA-3 (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |

Total \$106,168.00
Figure 3.8.11 - Redesign Cost Information for DR-2 Panel

| DR-3Equipment Costs for Redesign |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equip | Means No. | No. of Feeders | Feeder <br> Length (CFL) | Per Unit Cost | Cost |
| 300A 3P, Breaker (480) | 0430 | N/A | N/A | \$2,708.00 | \$2,708.00 |
| (3) 350MCM, \#4G, 2.5 EMT | 2600 | 3 | 0.25 | \$967.00 | \$725.25 |
| 225kVA X-Fmr | 4930 | N/A | N/A | \$23,374.00 | \$23,374.00 |
| 2 sets (4) 350MCM, 1/0G, (2) 2.5 EMT | 2600 | 8 | 0.25 | \$967.00 | \$1,934.00 |
| 700A, 3P Breaker (208) | 0470 | N/A | N/A | \$5,780.00 | \$5,780.00 |
| DR-3 Panel (800A) | 0300 | N/A | N/A | \$3,580.00 | \$3,580.00 |
| 110A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) \#2, \#6G, 1.25 EMT | 1500 | 4 | 0.25 | \$235.00 | \$235.00 |
| RP-BS (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 125A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) \#1, \#6G, 1.25 EMT | 1550 | 4 | 1.5 | \$286.00 | \$1,716.00 |
| RP-BSA (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 150A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) 1/0, \#6G, 1.5 EMT | 1600 | 4 | 0.5 | \$344.00 | \$688.00 |
| RP-1SB (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
| 100A, 3P Breaker (208) | 0320 | N/A | N/A | \$456.00 | \$456.00 |
| (4) \#3, \#8G, 1.25 EMT | 1450 | 4 | 0.75 | \$196.00 | \$588.00 |
| RP-2SB (100A) | 3110 | N/A | N/A | \$673.00 | \$673.00 |
| 175A, 3P Breaker (208) | 0420 | N/A | N/A | \$1,239.00 | \$1,239.00 |
| (4) 2/0, \#6G, 2 EMT | 1650 | 4 | 1 | \$419.00 | \$1,676.00 |
| RP-3SB (225A) | 3120 | N/A | N/A | \$955.00 | \$955.00 |
|  |  |  |  | Total | \$52,909.25 |

Figure 3.8.12 - Redesign Cost Information for DR-3 Panel

| System Redesign |
| :---: |
| Total Redesign Cost: $\quad \$ 263,788.25$ |

Figure 3.8.13 - Redesign Total Cost

## Analysis

The goals of the redesign were met although the cost of the redesign is approximately $\$ 43,000$ more than the original design. The redesign did reduce the number of transformers. It also resulted in smaller lighting panels because they are no longer serving multiple panels downstream. The ability to now put the transformers in the same room as its distribution panel reduces the long runs on the larger feeders. The primary side now is the longer run. The area in which the redesign fails is economics. Even though the number of transformers was reduced by five, because the new transformers are so much larger than the originals the cost is much greater. Also, distribution panels were added to the system which added cost. This cost was offset some by the reduction in size of the lighting panels.

An area that was not analyzed but would definitely be an issue is the physical size of the new transformers. The weight would have to be discussed with the structural engineer to ensure the structure could support them. Also, the dimension could quite possibly be too large to fit into some of the smaller electrical closets.

Overall, this system is more centralized and would be perhaps easier to install but the economics do not allow it to be considered as a feasible replacement for the system that is in place.

## ATRIUM HVAC EQUIPMENT POWER REDESIGN

## Introduction

The mechanical study that was done on the glazing in the atrium was intended to significantly change the power requirements for the air handling unit that conditions the atrium. However, the only significant change was the air handler's fan was reduced in size from 15 horse power to 7.5 horse power. This does not translate into a significant opportunity to reduce the power requirements to the air handling unit.

This section will focus on the redesign of the electrical components that serve AHU-1-R1. The panelboard that is affected by the air handling unit resizing is LP-3N which is located in Electrical Room 366 on the third floor. Panelboards for both the original system and the redesigned system will be presented. Panelboard sizing worksheets and feeder worksheets are also provided in this section.

## Redesign Procedure



Figure 4.1.1 - LP-3N Original Panelboard Worksheet


Figure 4.1.2 - LP-3N Original Panelboard Schedule


Figure 4.1.3 - LP-3N Redesign Panelboard Worksheet

Jason Greer I Villanova University: School of Law


Figure 4.1.4 - LP-3N Redesign Panelboard Schedule

## Summary



Figure 4.1.5 - LP-3N Redesign Summary

## Analysis

Even though the size of the air handling unit's fan was reduce by half from 15 hp to 7.5 hp , the effect on the electrical system was almost zero. The total reduction in design load amps was less than eleven which resulted in zero change for the breaker, conductors, or conduit.

Because of the simplicity of the previous electrical study and the lack of results it produced, I decided it would be worthwhile to explore an additional electrical topic in this report. The next section will focus on that.

## ENERGY EFFICIENT TRANSFORMER STUDY

## Introduction

The following section of this report explores the benefits and feasibility of implementing PowerSmiths T1000-C3 energy efficient transformers. The law school currently uses standard Krated transformers. An energy savings payback analysis will be done using PowerSmiths ESP Calculator.

The existing transformers in the law school are listed below:

| ORIGINAL TRANSFORMER SCHEDULE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TAG | PRIMARY VOLTAGE | $\begin{gathered} \text { SECONDARY } \\ \text { VOLTAGE } \end{gathered}$ | SIZE | TYPE | $\begin{gathered} \text { TEMP. } \\ \text { RISE } \end{gathered}$ | TAPS | MOUNTING | REMARKS |
| XD-1 | 13.2kV, 3P, 3W | 480Y/277V, 3P, 4W | 1500kVA | Silicone-based dielectric filled | $55^{\circ} \mathrm{C}$ | (4) $2.5 \%$ Taps (2) Up \& (2) Dn | Concrete Pad Mount (outside) |  |
| XS-1 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-2 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-3 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-4 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-5 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-6 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 30kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \% \mathrm{Taps}$ <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-7 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 75 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-8 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-9 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-10 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 45kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |
| XS-11 | 480Y/277V, 3P, 4W | 208Y/120V, 3P, 4W | 112.5 kVA | Dry Type | $115^{\circ} \mathrm{C}$ | (6) $2.5 \%$ Taps <br> (2) Up \& (4) Dn | Pad mounted, vibration isolated |  |

Figure 5.1.1 - Standard Transformer Schedule

The cost analysis was completed using a standard markup value of $25 \%$ for PowerSmiths transformers. This markup value was obtained from a PowerSmiths representative and was given as an estimated markup value.

## The ESP Calculator ${ }^{T M}$

Toll Free : 1-800-747-9627 or (905) 791-1493 Project Description Date

Energy Savings Payback Calculator
Villanova University: School of Law
April 4, 2008


Available Full Load kW
Average kVA (calc) equipment operating hrs/ day equipment operating days/yr Load during normal operating hours Load outside operating hours

Annual Cost to Operate Load Only kWh rate
demand rate (\$/kW/mo) ex. $\$ 10.00$

Annual Cost of Status Quo Transformer Losses \& Associated Air Conditioning (A/C) burden
Status quo Efficiency (Normal Operation)
Transformer kW Losses (Normal Operation)
Status quo Efficiency (Outside op. hrs)
Transformer kW Losses (Outside op. hrs)
Annual addititional kWh from transformers
Annual Cost of Transformer Losses
A/C System Performance (kW/ton) Additional Tons of Cooling (on peak)
Annual addititional kWh from A/C
Annual Cost of Associated A/C
Summary with Status Quo Transformer
Annual Cost of feeding Building Load
Annual Cost of Transformer Losses
Annual Cost of Associated A/C Electrical Bill (Status Quo Transformer)

92.0\%
93,093 kWh

IMPORTANT: By using the ESP Calculator ${ }^{T M}$, you are agreeing the TERMS OF USE section on page 3 Powersmiths International Corp. is a licensed user. Content subject to change without notice


Summary of Environmental Benefits

| Annual Reduction in Greenhouse Gases (per EPA) |
| :--- | ---: | ---: |
| 50 tons of CO2 |
| 163 tons of Coal |

## Conclusion

As a way to save energy, PowerSmiths T1000-C3 energy efficient transformers are a good option. The initial cost difference between the standard K-rated transformers that are currently in the building and the T1000-C3 series transformers is $\$ 3,360$. Thanks to the energy savings receive when using the T1000-C3 transformers, in just over seven years, the initial increase in cost will have been paid back.

Perhaps more importantly than the money that can be saved are the environmental savings. Each year, running the energy efficient transformers will reduce the CO 2 released into the atmosphere by 50 tons or replaced 163 tons of burned coal. This translates into planting nine acres of trees or eliminating the emissions of seven cars for the year.

Implementation of the T1000-C3 transformers is a feasible design idea. Not only will the energy cost required to operate the law school be greatly reduced, the buildings annual environmental impact is greatly reduced.

## PROTECTION DEVICE COORDINATION

## Introduction

The protective device coordination focuses on the over-protection devices along the path from main switchgear through panel ELP-1S. The devices are studied to determine if they are coordinated correctly and will operate as planned in the case of a fault.

## Partial Single Line of Path

The devices that are analyzed for this protective device coordination study are: a 400 amp circuit breaker located in the main switchboard (MDB), the 100 amp main circuit breaker in panel EDP-BS and through a 50 amp breaker in panel EDP-BS.


Figure 6.1.1 - Protection Coordination Path

The time/current trip curve for each device shown above was overlaid to illustrate the coordination of the devices.


Figure 6.1.2 - Time/Current Overlay

## Conclusion

The 225A circuit breaker is coordinated correctly; it will never trip before either of the smaller overcurrent devices. The 100A and 50A breakers however, are not coordinated quite right. At low currents the 50 amp breaker will always trip first as it should. When the current increases however, there comes a point where there is the possibility of the 100 amp breaker tripping before the 50 amp breaker. The point at which this occurs is where the red and blue curves intersect. At one point, the blue curve is further to the right than the red which means at that point, there is a real possibility of the larger breaker tripping first. This is a problem if there are other loads connected to the larger breaker because if that trips before the branch circuit, all loads will be lost, not just the one that has the fault.

## Mechanical Breadth

## Introduction

In an effort to lessen the harsh daylight glare and to reduce solar gains in the atrium, new glazing was assigned and a daylight and mechanical study was done. The daylight study can be seen starting on page 31 of this report. The following section focuses on the mechanical improvements the newly assigned glazing provides the law school.

The original mechanical engineer who modeled the building initially assumed that the spandrel glass would behave like a brick wall with a U-value of 0.0725 BTU/h- $\mathrm{ft} \wedge 2-\mathrm{F}$. Because Viracon does not list the properties of coating material (most likely because it is coated by an outside company), I continued that same assumption.

The redesigned glazing system implements glazing with lower transmittance values and lower shading coefficients. Both of these things result in a lower relative heat gain. The two glazing systems were calculated using Trane Trace 700. The reduction in loads and energy consumption will be discussed below. Finally, an annual energy savings is discussed along with the increase in construction cost due to the new glazing system.

Glazing

| Original Atrium Glazing |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Viracon No. | Description | Vis. Light | Transmitta Solar Energy | ance <br> Ultra- <br> Violet | Vis. Light-Ext. | Reflectance Vis. Light-Int. | Solar <br> Energy | ASHRAE <br> Winter Night | U-Value Summer Day | Shading Coeff. | Relative Heat Gain | Area (SF) |
| VRE 1-38 | Solarscreen (clear) | 36\% | 19\% | 12\% | 44\% | 21\% | 46\% | 0.25 | 0.21 | 0.26 | 55 | 880 |
| VRE 1-38 Frit | Silkscreen (dots) | 25\% | 13\% | 7\% | 40\% | 25\% | 13\% | 0.30 | 0.26 | 0.21 | 46 | 2592 |
| VE 1-2M w/ Metallic Opac | Spandrel | 0\% | Not Avail. | Not Avail. | Not Avail. | Not Avail. | Not Avail. | 0.07 | 0.07 | N/A | Not Avail. | 674 |
| New Atrium Glazing |  |  |  |  |  |  |  |  |  |  |  |  |
| Viracon No. | Description | Vis. Light | Transmitta Solar Energy | ance <br> Ultra- <br> Violet | Vis. <br> Light-Ext. | Reflectance <br> Vis. <br> Light-Int. | Solar <br> Energy | ASHRAE U-Value |  | Shading Coeff. | Relative Heat Gain | Area (SF) |
| VRE 7-38 | Solarscreen (clear) | 28\% | 11\% | 9\% | 28\% | 21\% | 14\% | 0.25 | 0.21 | 0.19 | 41 | 880 |
| VRE 1-38 Frit | Silkscreen (dots) | 19\% | 8\% | 5\% | 26\% | 24\% | 13\% | 0.30 | 0.26 | 0.17 | 37 | 1795 |
| VE 1-2M w/ Metallic Opac | Spandrel | 0\% | Not Avail. | Not Avail. | Not Avail. | Not Avail. | Not Avail. | 0.07 | 0.07 | N/A | Not Avail. | 1471 |

Table 7.1.1 - Glazing Properties
*See Appendix E for Glazing Cutsheets

## Redesign Details

The redesign of the atrium glazing consisted of adding additional spandrel glass, which resulted in a reduction in fritted glass. The amount of clear glass remained the same. As seen in the table above, all VRE 1-38 glazing was replaced with VRE 7-38.


Figure 7.1.1 - Original Glazing Detail


Figure 7.1.1 - Redesign Glazing Detail

| VU Atrium Mechanical Cost Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathscr{0} \\ & \frac{\tilde{\sigma}}{\top} \end{aligned}$ |  |  | Viracon No. |  |  | Area (SF) |  | Unit Cost (\$/SF) |  | Initial Cost |  |  |
|  | Tag | Description | Original | Redesign | Add-ons | Original | Redesign | Original | Redesign | Original | Redesign | Cost Diff. |
|  | GL-2 | Silkscreen (dots) | VRE 1-38 | VRE 7-38 | Dots | 2539 | 1742 | \$18.50 | \$21.00 | \$46,971.50 | \$36,582.00 | 10,389.50 |
|  | GL-3 | Spandrel | VE 1-2M | VE 1-2M | Metallic Opac | 674 | 1471 | \$24.00 | \$24.00 | \$16,176.00 | \$35,304.00 | -19,128.00 |
|  | GL-4 | Solarscreen(clear) | VRE 1-38 | VRE 7-38 | N/A | 880 | 880 | \$12.50 | \$15.00 | \$11,000.00 | \$13,200.00 | -2,200.00 |
|  |  |  |  |  |  |  |  | Total Gla | ss Cost | \$74,147.50 | \$85,086.00 | -10,938.50 |
| \|고 |  |  | Trane Series |  |  | Initial Cost |  |  |  |  |  |  |
|  | Tag | Description | Original | Redesign | Add-ons | Original | Redesign | Cost Diff. |  |  |  |  |
|  | AHU-R-1 | Rooftop AHU | $\begin{aligned} & \begin{array}{l} \text { Trane T-25 } \\ (15 \mathrm{hp}) \end{array} \\ & \hline \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \text { Trane T-12 } \\ (7.5 \mathrm{hp}) \end{array} \\ & \hline \end{aligned}$ | N/A | \$25,990.00 | \$22,190.00 | \$3,800.00 |  |  |  |  |
| Construction Cost Difference - $\$ 7,138.50$ |  |  |  |  |  |  |  |  |  |  |  |  |

Note: Glazing and AHU pricing was provide by Viracon and Trane representative respectively.
Table 7.1.2 - Construction Cost Analysis

| AHU-1-R1 |  |  |
| :---: | :---: | :---: |
| Peak Design Cooling Load | Original Glazing 22.7 ton | Redesigned Glazing 16.2 ton |
| Peak Design Heating Load | 147 MBh | 108 MBh |
| Outside Airflow | 1316 cfm | 894 cfm |
| Cooling Airflow | 8873 cfm | 6059 cfm |
| Heating Airflow | 8873 cfm | 6059 cfm |
| Return Airflow | 8873 cfm | 6059 cfm |
| Exhaust Airflow | 8873 cfm | 6059 cfm |
| AHU Fan Size | 15 hp | 7.5 hp |
| \% of Total Building Energy: Heating | 37.20\% | 37.10\% |
| \% of Total Building Energy: Cooling | 13.30\% | 13.40\% |
| Total Building Energy | 15172882 kBtu/yr | 15058292 kBtu/yr |
| Total Energy Savings | 114590 kBtu/yr |  |
| Total Electricity Cost | \$44,064 | \$43,690 |
| Total Electricity Cost Savings | \$374 per year |  |

Table 7.1.3 - AHU Properties and Energy Savings

## Conclusion

The change in glazing seems to have had more benefits for daylighting than the mechanical system. The reduction in shading coefficient and transmittance did make an impact, but it turned out to be small compared to the load of the rest of the building. The annual electricity savings only amounted to $\$ 374$. The law school is heated using steam like Penn State's buildings are. I could not estimate the annual savings for the steam because I did not know where or how the steam was produced. Judging by the electricity savings compared to the percentage change in cooling, I am confident saying that the savings would not be incredibly significant.

Implementation of the new glazing system would result in an increased construction cost of approximately $\$ 11,000$. This is a result of the VRE 7-38 being more expensive than the originally specified VRE 1-38 and the increase square footage of VE 1-2M. This cost was offset some by the reduction in air handler size. AHU-1-R1 was originally a Trane T- 25 with a 15 horse power fan. The reduction in load for the atrium allowed the air handler to be reduced to a Trane T-12 with a 7.5 horse power fan. The cost difference between the two was estimated at $\$ 3,800$. The combination of the new glazing and new air handler result in a net construction cost increase of $\$ 7,138.50$.

Because the yearly energy savings is not significant, this cost would most likely have to be presented to the owner as a necessary cost to improve the daylight conditions in the atrium and not as a way to save money on energy costs. Because the VU law school costs upwards of $\$ 56$ million, a $\$ 7,000$ increase may be a justified price to improve the daylighting in the atrium.

## Acoustical Breadth

## Introduction

In both the moot courtroom and the 135 -seat classroom, wood is a very dominant material. Because both spaces are used primarily for lectures and presentations, hearing the spoken word is very important for this space.

Because of the amount of wood, this acoustical breadth was decided upon on the assumption that the room would have a reverberation time that is higher than the recommended time. This report will show however, that the acoustical measures that were taken in the initial design lowered the reverberation time past the recommended range.

Once the materials that needed to be added or removed to reach the recommended reverberation time were determined, a cost analysis was done. The purpose of the cost analysis was to ensure that the changes that were necessary to bring each space back into the recommended range was feasible economically.

## Moot Court



The existing conditions for the moot court for each frequency shown produce a reverberation time range from 0.46 seconds at 4000 Hz to 0.64 seconds at 125 Hz . The acceptable range this space is 0.7 to 1.1 seconds. The courtroom has acoustical panels and acoustical ceiling tile. Those are the materials that will be changed in order to get this space inside the recommended reverberation time range.

| Surface Description |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Material | Surface Area |  |  |  |  | rp | Co | icien | and |  |  |  |  |
|  |  |  | 125 Hz |  | 250 Hz |  | 500 Hz |  | 1000 Hz |  | 2000 Hz |  | 4000 Hz |  |
|  |  |  | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A |
| Floor | Carpet, light, foam-backed | 2013 | 0.05 | 100.65 | 0.10 | 201.30 | 0.12 | 241.56 | 0.30 | 603.90 | 0.40 | 805.20 | 0.50 | 1006.50 |
| Ceiling 1 | 1/2" Gyp Board | 375 | 0.11 | 41.25 | 0.11 | 41.25 | 0.05 | 18.75 | 0.06 | 22.50 | 0.04 | 15.00 | 0.05 | 18.75 |
| Ceiling 2 | 1/2" Gyp Board | 790 | 0.11 | 86.90 | 0.11 | 86.90 | 0.05 | 39.50 | 0.06 | 47.40 | 0.04 | 31.60 | 0.05 | 39.50 |
| Ceiling 3 | 1/2" Gyp Board | 854 | 0.11 | 93.94 | 0.11 | 93.94 | 0.05 | 42.70 | 0.06 | 51.24 | 0.04 | 34.16 | 0.05 | 42.70 |
| Ceiling 4 | 1/2" Gyp Board | 410 | 0.11 | 45.10 | 0.11 | 45.10 | 0.05 | 20.50 | 0.06 | 24.60 | 0.04 | 16.40 | 0.05 | 20.50 |
| Walls | 1/2" Gyp Board on Studs | 1758 | 0.27 | 474.66 | 0.10 | 175.80 | 0.05 | 87.90 | 0.04 | 70.32 | 0.03 | 52.74 | 0.03 | 52.74 |
| Desk Tops | Wood | 363 | 0.10 | 36.30 | 0.11 | 39.93 | 0.10 | 36.30 | 0.08 | 29.04 | 0.08 | 29.04 | 0.11 | 39.93 |
| Desk Front/Sides | Wood | 482 | 0.10 | 48.20 | 0.11 | 53.02 | 0.10 | 48.20 | 0.08 | 38.56 | 0.08 | 38.56 | 0.11 | 53.02 |
| Bench Top | Wood | 52 | 0.10 | 5.20 | 0.11 | 5.72 | 0.10 | 5.20 | 0.08 | 4.16 | 0.08 | 4.16 | 0.11 | 5.72 |
| Chair | Light Upholstry | 810 | 0.35 | 283.50 | 0.45 | 364.50 | 0.57 | 461.70 | 0.61 | 494.10 | 0.59 | 477.90 | 0.55 | 445.50 |
| Door | Wood | 168 | 0.10 | 16.80 | 0.11 | 18.48 | 0.10 | 16.80 | 0.08 | 13.44 | 0.08 | 13.44 | 0.11 | 18.48 |
| Interior Walls | Wood | 315 | 0.10 | 31.50 | 0.11 | 34.65 | 0.10 | 31.50 | 0.08 | 25.20 | 0.08 | 25.20 | 0.11 | 34.65 |
| Tables | Wood | 112 | 0.10 | 11.20 | 0.11 | 12.32 | 0.10 | 11.20 | 0.08 | 8.96 | 0.08 | 8.96 | 0.11 | 12.32 |
| Front Wood Panelling | 1" Wood Panelling | 242 | 0.19 | 45.98 | 0.14 | 33.88 | 0.09 | 21.78 | 0.06 | 14.52 | 0.06 | 14.52 | 0.05 | 12.10 |
| Witness Chair | Wood | 12 | 0.10 | 1.20 | 0.11 | 1.32 | 0.10 | 1.20 | 0.08 | 0.96 | 0.08 | 0.96 | 0.11 | 1.32 |
| Witness Railing | Wood | 25 | 0.10 | 2.50 | 0.11 | 2.75 | 0.10 | 2.50 | 0.08 | 2.00 | 0.08 | 2.00 | 0.11 | 2.75 |
| Railing | Wood | 60 | 0.10 | 6.00 | 0.11 | 6.60 | 0.10 | 6.00 | 0.08 | 4.80 | 0.08 | 4.80 | 0.11 | 6.60 |
| Acoustical Panels | 2" Acoustic Panel | 125 | 0.27 | 33.75 | 0.55 | 68.75 | 1.07 | 133.75 | 1.10 | 137.50 | 1.10 | 137.50 | 1.10 | 137.50 |
| EA |  |  | 1364.63 |  | 1286.21 |  | 1227.04 |  | 1593.20 |  | 1712.14 |  | 1950.58 |  |
| Volume (ft ${ }^{3}$ ) | $26,675$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Reverb Time (s) | $\mathrm{T}_{60}=0.049 \mathrm{~V} / \Sigma \mathrm{A}$ |  | 0.96 |  | 1.02 |  | 1.07 |  | 0.82 |  | 0.76 |  | 0.67 |  |
| Target Time (s) | 0.7-1.1 |  | Acceptable |  | Acceptable |  | Acceptable |  | Acceptable |  | Acceptable |  | Unacceptable |  |

By eliminating all acoustical ceiling tile and reducing the surface area of the acoustical panels on the perimeter from 194 square feet to 125 square feet, all frequencies except for 4000 Hz now fall within the acceptable range of 0.7 to 1.1 seconds of reverberation time. Because lower frequencies resonate longer, it is easier to get those to fall into the recommended range. It is more difficult to do so with the higher frequencies because they die out much quicker than low pitched sounds.

In the acoustical redesign of the moot court, the 4000 Hz frequency was left at 0.67 seconds of reverberation time because it is close to the accepted value. Also, in order to have the 4000 Hz frequency fall within the recommended range, the 500 Hz frequency would have then been past the upper limit of the recommended range.

## 135-Seat Classroom

| Surface Description $\quad$ Material $\begin{gathered}\text { 135-Sea } \\ \\ \text { Surface } \\ \text { Area }\end{gathered}$ |  |  | 125 Hz |  | Absorption Coefficient and Sabins $500 \mathrm{~Hz}$ <br> 1000 Hz |  |  |  |  |  | 2000Hz |  | 4000Hz |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A |
| Floor | Carpet, light, foam-backed | 3085 | 0.05 | 154.25 | 0.10 | 308.50 | 0.12 | 370.20 | 0.30 | 925.50 | 0.40 | 1234.00 | 0.50 | 1542.50 |
| High Ceiling | 5/8" Acoustical Tile | 2280 | 0.68 | 1550.40 | 0.76 | 1732.80 | 0.60 | 1368.00 | 0.65 | 1482.00 | 0.82 | 1869.60 | 0.76 | 1732.80 |
| Low Ceiling | 1/2" Gyp Board | 866 | 0.11 | 95.26 | 0.11 | 95.26 | 0.05 | 43.30 | 0.06 | 51.96 | 0.04 | 34.64 | 0.05 | 43.30 |
| Walls | $\begin{aligned} & \text { 1/2" Gyp Board } \\ & \text { on Studs } \end{aligned}$ | 2149 | 0.27 | 580.23 | 0.10 | 214.90 | 0.05 | 107.45 | 0.04 | 85.96 | 0.03 | 64.47 | 0.03 | 64.47 |
| Desk Tops | Wood | 1563 | 0.10 | 156.30 | 0.11 | 171.93 | 0.10 | 156.30 | 0.08 | 125.04 | 0.08 | 125.04 | 0.11 | 171.93 |
| Desk Front/Sides | Wood | 1028 | 0.10 | 102.80 | 0.11 | 113.08 | 0.10 | 102.80 | 0.08 | 82.24 | 0.08 | 82.24 | 0.11 | 113.08 |
| Chair | Light Upholstry | 1890 | 0.35 | 661.50 | 0.45 | 850.50 | 0.57 | 1077.30 | 0.61 | 1152.90 | 0.59 | 1115.10 | 0.55 | 1039.50 |
| Door | Wood | 126 | 0.10 | 12.60 | 0.11 | 13.86 | 0.10 | 12.60 | 0.08 | 10.08 | 0.08 | 10.08 | 0.11 | 13.86 |
| Ramp Walls | $\begin{aligned} & \text { 1/2" Gyp Board } \\ & \text { on Studs } \end{aligned}$ | 85.5 | 0.27 | 23.09 | 0.10 | 8.55 | 0.05 | 4.28 | 0.04 | 3.42 | 0.03 | 2.57 | 0.03 | 2.57 |
| Acoustical Panels | 2" Acoustic Panel | 248 | 0.27 | 66.96 | 0.55 | 136.40 | 1.07 | 265.36 | 1.10 | 272.80 | 1.10 | 272.80 | 1.10 | 272.80 |
| £A |  |  |  | 3.39 |  | 45.78 |  | 7.59 |  | 1.90 |  | 10.54 |  | 6.81 |
| Volume ( $\mathrm{ft}^{3}$ ) | 40,105 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Reverb Time (s) | $\mathrm{T}_{60}=0.049 \mathrm{~V} / \Sigma \mathrm{A}$ |  |  | . 58 |  | . 54 |  | . 56 |  | . 47 |  | 0.41 |  | . 39 |
| Target Time (s) | 0.7-1.1 |  | Unac | eeptable | Unac | eptable | Unac | eptable | Unac | eptable | Unac | ceptable | Una | ceptable |

The classroom has many of the same materials as the courtroom and therefore has similar acoustical problems. The reverberation time range for the classroom was calculated at 0.39 seconds for 4000 Hz frequencies up to 0.58 seconds at 125 Hz . Again, the means for getting the reverberation times into the acceptable range will be to reduce the amount of acoustical materials that are in the classroom.

| Surface Description $\quad$ Material $\begin{gathered}\text { 135-Seat } \\ \\ \\ \\ \text { Surface } \\ \text { Area }\end{gathered}$ |  |  | assroom125 Hz |  | 250 Hz |  | Time Calculations bsorption Coefficient and Sabins500Hz$1000 \mathrm{~Hz}$ |  |  |  | 2000Hz |  | 4000Hz |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A | $\alpha$ | A |
| Floor | Carpet, light, foam-backed | 3085 | 0.05 | 154.25 | 0.10 | 308.50 | 0.12 | 370.20 | 0.30 | 925.50 | 0.40 | 1234.00 | 0.50 | 1542.50 |
| High Ceiling | 1/2" Gyp Board | 2280 | 0.11 | 250.80 | 0.11 | 250.80 | 0.05 | 114.00 | 0.06 | 136.80 | 0.04 | 91.20 | 0.05 | 114.00 |
| Low Ceiling | 1/2" Gyp Board | 866 | 0.11 | 95.26 | 0.11 | 95.26 | 0.05 | 43.30 | 0.06 | 51.96 | 0.04 | 34.64 | 0.05 | 43.30 |
| Walls | $\begin{aligned} & \hline \text { 1/2" Gyp Board } \\ & \text { on Studs } \\ & \hline \end{aligned}$ | 2149 | 0.27 | 580.23 | 0.10 | 214.90 | 0.05 | 107.45 | 0.04 | 85.96 | 0.03 | 64.47 | 0.03 | 64.47 |
| Desk Tops | Wood | 1563 | 0.10 | 156.30 | 0.11 | 171.93 | 0.10 | 156.30 | 0.08 | 125.04 | 0.08 | 125.04 | 0.11 | 171.93 |
| Desk Front/Sides | Wood | 1028 | 0.10 | 102.80 | 0.11 | 113.08 | 0.10 | 102.80 | 0.08 | 82.24 | 0.08 | 82.24 | 0.11 | 113.08 |
| Chair | Light Upholstry | 1890 | 0.35 | 661.50 | 0.45 | 850.50 | 0.57 | 1077.30 | 0.61 | 1152.90 | 0.59 | 1115.10 | 0.55 | 1039.50 |
| Door | Wood | 126 | 0.10 | 12.60 | 0.11 | 13.86 | 0.10 | 12.60 | 0.08 | 10.08 | 0.08 | 10.08 | 0.11 | 13.86 |
| Ramp Walls | $\begin{aligned} & \text { 1/2" Gyp Board } \\ & \text { on Studs } \\ & \hline \end{aligned}$ | 85.5 | 0.27 | 23.09 | 0.10 | 8.55 | 0.05 | 4.28 | 0.04 | 3.42 | 0.03 | 2.57 | 0.03 | 2.57 |
| Acoustical Panels* | 2" Acoustic Panel | 86 | 0.27 | 23.22 | 0.55 | 47.30 | 1.07 | 92.02 | 1.10 | 94.60 | 1.10 | 94.60 | 1.10 | 94.60 |
| EA |  |  | 2060.05 |  | 2074.68 |  | 2080.25 |  | 2668.50 |  | 2853.94 |  | 3199.81 |  |
| Volume ( $\mathrm{ft}^{3}$ ) | 40,105 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Reverb Time (s) | $\mathrm{T}_{60}=0.049 \mathrm{~V} / \Sigma \mathrm{A}$ |  | 0.95 |  | 0.95 |  | 0.94 |  | 0.74 |  | 0.69 |  | 0.61 |  |
| Target Time (s) | 0.7-1.1 |  | Acceptable |  | Acceptable |  | Acceptable |  | Acceptable |  | Unacceptable |  | Unacceptable |  |

*Note: Originally there were three 22SF panels on each side wall and eight 14.4 SF panels on the back wall. The new design is one 14.4 SF on each side wall with four 14.4SF panels on the back wall.

By replacing the acoustical ceiling tile with painted gyp board and reducing the number and size of acoustical panels on the side and back walls, the reverberation time was brought into the recommended range for the four lowest frequencies and much closer for 2000 and 4000 Hz . The 2000 Hz frequencies miss falling within the acceptable range by one one-hundredth of a second while 4000 Hz frequencies miss by nine one-hundredths of a second. If the acoustical panels would
have been eliminated all together, the 2000 Hz frequencies would have fallen in the range but because these are used as an architectural feature in the lighting design, they it was deemed important to leave a few of them. Even if they were eliminated all together, the 4000 Hz frequencies would have still be just outside the recommended range for reverberation time.

## Cost Analysis

| Moot Court Redesign Cost Calculation |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Surface Description | Material |  | Surface Area |  | RS Means Unit Cost (\$/SF) |  | RS Means Cost |  | Redesign Saving |
|  | Original | Redesign | Original | Redesign | Original | Redesign | Original | Redesign |  |
| Ceiling 1 | 5/8" Acoustical Tile | 1/2" Gyp Board | 375 | 375 | \$1.85 | \$1.25 | \$693.75 | \$468.75 | \$225.00 |
| Ceiling 2 | 5/8" Acoustical Tile | 1/2" Gyp Board | 790 | 790 | \$1.85 | \$1.25 | \$1,461.50 | \$987.50 | \$474.00 |
| Acoustic Wall Panels | 2" Acoustic Panel | 2" Acoustic Panel | 194 | 125 | \$5.00 | \$5.00 | \$970.00 | \$625.00 | \$345.00 |

Moot Court Redesign Total Savings
Total Savings = \$1,044.00

| Surface Description | 135-Seat Classroom Redesign Cost Calculation |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Material |  | Surface Area |  | RS Means Unit Cost (\$/SF) |  |  | RS Means Cost |  | Redesign Saving |
|  | Original | Redesign | Original | Redesign | Original | Redesign |  | Original | Redesign |  |
| High Ceiling | 5/8" Acoustical Tile | 1/2" Gyp Board | 2280 | 2280 | \$1.8 |  | \$1.25 | \$4,218.00 | \$2,850.00 | \$1,368.00 |
| Acoustic Wall Panels | 2" Acoustic Panel | 2" Acoustic Panel | 248 | 86 | \$5.00 |  | \$5.00 | \$1,240.00 | \$430.00 | \$810.00 |
| 135-Seat Classroom Redesign Total Savings <br> Total Savings = \$2,178.00 |  |  |  |  |  |  |  |  |  |  |

Each acoustical redesign resulted in a net savings because of the reduction in acoustical material. If both redesigns would to be implemented into the construction of the law school, the total construction costs would be reduced by $\$ 3,222$.

## Conclusion

Implementing the new design would meet the goals laid out in the initial plan. The room would perform better acoustically and it would actually be cheaper than the original system. This is a system that could feasibly be introduced into this building.

## Summary and Conclusions

## Lighting Depth

Each of the four spaces that were redesigned met ASHRAE 90.1 power density criteria. The overall lighting goals were based around the need to create functional education spaces. However, the architecture of the law school has some excellent features that were perfect for the focus of a lighting design. The atrium was transformed into a glowing beacon that will grace Villanova University as a new part of its skyline. The more interior spaces also had architectural features that presented some excellent lighting opportunities. The courtroom and classroom each have a great amount of wood as well as interesting ceilings. These two elements made lighting the space that much more challenging and as a result, the spaces are that much more interesting. Finally, from outside to inside, the emphasis on the rich materials and elegant architecture allows the prestige and excellence of the law school and the ideals of the legal profession to shine through.

A daylight study was conducted on the atrium because of the large amount of south-east facing glazing. The original glazing was replaced with glazing that had a lower shading coefficient and lower transmittance. Calculations were run and it was determined that the new glass would reduce the illuminance on the atrium floor as well as lessen the depth of the penetration of direct sunlight into the space.

## Electrical Depth

The electrical depth explored a few different concepts including coordination of electrical system and the newly designed lighting systems, a distribution redesign, a mechanical equipment power redesign, a study of energy efficient transformers and a protective device coordination study.

The lighting coordination consisted of re-circuiting of lighting branch circuits and adjusting the panelboards accordingly. A few of the panels were not sized to adequately handle the loads that were listed according to the panelboard schedules that were used in sizing. As a result, a few of the panels increased in size. The majority of panelboards however, remained the same because the lighting loads that were changed were not changed significantly and the same panels were used whenever possible.

The distribution redesign had great potential but in the end, it turned out that the redesign reduced the number of transformers but increased the size of those transformers which does not translate into cost savings. Also, the addition of distribution panels and large circuit breakers increased the cost of the new system which turned out to be too expensive to be considered feasible.

The HVAC system redesign consisted of redesigning the power supply to a rooftop air handling unit. The air handling unit was resized per the mechanical breadth, but the resizing did not significantly affect the electrical system. The panel, breakers and feeders did not change in size as a result of the resizing of the air handler. As a result of these poor results, an additional study was performed.

The additional study that was performed was a payback calculation of replacing standard K-rated transformers with PowerSmiths energy efficient transformers. It was found that after only seven
years, the additional cost for the transformers would be reclaimed through the annual energy savings provided by the transformers.

## Mechanical Breadth

The goal of the mechanical breadth was to reduce the mechanical loads of the building by changing the glazing in the atrium. After an analysis was performed, the glazing that was chosen did reduce mechanical loads, but it was not significant. The glass that was originally specified was actually very good so it was difficult to find something that performed much better. In the scope of the whole building, the reduction in mechanical loads produced by the substitution of atrium glass did not make much of an impact. The glazing did a better job for the daylight system than it did for the mechanical system.

## Acoustical Breadth

The acoustical breadth was proposed because it was assumed that the amount of hard surfaces such as wood in the classroom and courtroom would have produced a reverberation time that was out of the recommended range on the high side. Upon completion of the study however, it was determined that the acoustical provisions that were designed into the building were keeping the reverberation time out of the recommended range on the low side. In each case, the amount of acoustical materials in the room was reduced and the reverberation time came much closer to falling in the recommended range. Lastly, a cost analysis was done and it was determined that replacing the acoustic ceiling tile and reducing the number of acoustical panels on the walls would save the project money.

## References

2005 National Electric Code. Nation Fire Protection Association. 2005.
ASHRAE Standard 90.1-2004. American Society of Heating, Refrigerating and Air Conditioning Engineers, Inc. Atlanta, Ga. 2004.

CMD Group. Romans Electrical Cost Data 2008. Kensington, MA. R.S. Means Company, Inc., 2008

Hughes, David. Electrical Systems in Buildings. Delmar Publishers Inc. Albany, NY. 1988.
Long, Marshall. Architectural Acoustics. Elsevier Inc. Burlinton, MA. 2006
Mehta, Madan, et. al. Architectural Acoustics: Principles and Design. Prentice-Hall, Inc. Upper Saddle River, New Jersey. 1999.

Rae, Mark S., ed. The IESNA Lighting Handbook: Reference \& Application, Ninth Edition. Illuminating Engineering Society of North America. New York. 2000.

## Acknowledgements

Thanks to everyone who has helped me throughout the course of senior thesis. All the help, knowledge, support has been so important in my completion of this capstone project.

## Companies

SmithGroup
Viracon
Trane
Villanova University
PowerSmiths

Individuals

Il Kim of SmithGroup
Jack Mahoney of SmithGroup
Brad Hartman of SmithGroup
AE Faculty
Dr. Mistrick
Professor Dannerth
Dr. Houser
Professor Parfitt
Professor Holland
And thank you to all my friends and family for their understanding and support through this long and sometimes difficult process.

